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4 **1 Temporary feeding shocks increase the productivity in a continuous**
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7 **2 biohydrogen producing reactor**
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26 data from the reactors.

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4 **27 Abstract**
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10 **29** Continuous hydrogen production stability and robustness by dark
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12 **30** fermentation were comprehensively studied at laboratory scale. Continuous
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15 **31** bioreactors were operated at two different hydraulic retention times (HRT) of 6 and
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17 **32** 10 hours. The reactors were subjected to feeding shocks given by decreases in the
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20 **33** HRT, and therefore the organic loading increase, during 6 and 24 hours. **Results**
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22 **34** indicated that the H₂ productivity was significantly improved by the temporary
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25 **35** organic shock loads, increasing the hydrogen production rate up to 40%, compared
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28 **36** to the rate obtained at the steady-state condition. Besides, it was observed that after
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31 **37** the shock load, the stability of the reactor (measured as the hydrogen production
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33 **38** rate) was recovered attaining the values observed before the feeding shocks. The
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36 **39** bioreactor operated at shorter HRT (6 h) showed better H₂ productivity (17.3 ± 1.1 L
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38 **40** H₂/L-d) in comparison to the other one operated at 10 h HRT (12.4 ± 1.6 L H₂/L-d).

41 **41**

42 **42 Keywords:** biohydrogen, CSTR, dark fermentation, feeding shock, HRT
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46 **43** perturbations, statistical analysis
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44 1. Introduction

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46 Dark fermentation has been extensively investigated in the past decades and
47 from a practical point of view, it became one of the most feasible methods for
48 biohydrogen production (Kumar et al. 2015). As a result of the significant progress
49 on these methods, the need of producing biohydrogen in continuous operation was
50 emphasized since it is preferred for future larger-scale implementations (Wang and
51 Wang 2009). Nevertheless, to accomplish sustainable biotechnological hydrogen
52 formation in continuous systems, several factors and process variables have to be
53 considered (Bakonyi et al. 2014). For instance, the selection, enrichment and
54 adaption of inoculum (Hernández-Mendoza and Buitrón 2014; Hernández-Mendoza
55 et al. 2014; Kumar et al. 2016), the reactor design (Bakonyi et al. 2014) and the
56 operating conditions e.g. hydraulic retention time (HRT) (Buitrón et al. 2014;
57 Bakonyi et al. 2015; Sivagurunathan et al. 2016).

58 Buitrón and Carvajal (2010) reported that short hydraulic retention times
59 increased the biohydrogen production. Specifically, Thanwised et al. (2012)
60 achieved a rise in hydrogen productivity (164 vs. 883 mL H₂/L-d) by switching the
61 HRT from 24 h to 6 h in an anaerobic baffled reactor. Also, Ramírez-Morales et al.
62 (2015) accomplished maximum mean hydrogen productivity of 23.4 L H₂/L-d at 6 h
63 of HRT in a continuous stirred tank reactor (CSTR). However, Park et al. (2015)
64 communicated that short hydraulic retention times could be seen as a threat given
65 that may cause the loss of precious H₂-forming biological activity. Shen et al. (2009)

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4 66 assessed the effect of the Organic Loading Rate (OLR) on the biohydrogen
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7 67 production using two reactor configurations (CSTR and a membrane bioreactor),
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10 68 achieving a maximum productivity of 4.25 LH₂/L-d at 30 g **chemical oxygen**
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12 69 **demand** (COD)/L-d in the CSTR, whilst the productivity was of 4.48 LH₂/L-d at 22
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15 70 g COD/L-d in the membrane bioreactor. [Hafez et al. \(2010\)](#) reported maximum H₂
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17 71 productivity of 35.6 L H₂/L-d at 103 g COD/L-d in a CSTR coupled to a clarifier.
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20 72 Later, [Zhang \(2014\)](#) accomplished maximum hydrogen productivity (22.8 L H₂/L-d)
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22 73 at approx. 85 g COD/L-d in a CSTR. Besides, [Ramírez-Morales et al. \(2015\)](#)
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25 74 evaluated the effect of OLR on the hydrogen production in a CSTR using glucose as
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28 75 substrate, and documented 25.4 L H₂/L-d **productivity** at 100 g COD/L-d.

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31 76 **Nevertheless**, the long-term stability of the fermenter is considerably
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33 77 dependent on the process conditions, mainly the HRT and the OLR. The possible
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36 78 vulnerability of continuous hydrogen fermenters was enlightened by
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39 79 [Baghchehsaraee et al. \(2011\)](#), revealed after careful experimentation that
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41 80 perturbations in the process associated with feed interruption could strongly affect
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44 81 the process stability and revival of bacteria. Hence, when extreme disturbances
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47 82 occur, the biosystem – depending on its robustness – may fail. Although the
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50 83 probability of operational disturbances under laboratory environment is expectably
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52 84 low because of the well-controlled input and process variables i.e. constant feed
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55 85 composition and feed flow rate, process disturbances could be notable when
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57 86 stepping out to a real and industrial case (**Fig. 1**). For instance, [Krupp and Widmann](#)
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59 87 ([2009](#)) pointed out that reliable feeding of the bioreactor could be challenging due to

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4 88 difficulties with (i) pumping, (ii) mixing or (iii) the supply of a consistent input
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7 89 stream. However, such aspects are scantily addressed in the literature.
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10 90 This work evaluates the continuous biohydrogen production by dark
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12 91 fermentation with a primary focus on the impact of organic shock loads associated
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15 92 with shifts in the HRT. Besides, the duration of these temporary feeding shocks as
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18 93 another variable of operational disturbance was assessed as well. Data and
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20 94 experiences about the influence of temporary process shocks could have a useful
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23 95 contribution to the design of future, scaled-up continuous processes for biohydrogen
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25 96 production.
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27 28 97 29 30 98 **2. Materials and Methods**

31 32 99 **2.1 Inoculum, culture medium and start-up**

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38 101 According to literature reports, the employment of diverse, mixed bacterial
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41 102 populations in completely stirred tank reactors is an attractive and widely-applied
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44 103 strategy to start-up and establish continuous hydrogen production ([Jung et al. 2011](#);
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46 104 [Show et al. 2011](#)). In this study, granular anaerobic sludge from a UASB reactor for
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49 105 wastewater treatment was used as inoculum after thermal pretreatment ([Buitrón and](#)
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52 106 [Carvajal, 2010](#)) for an H₂-producing CSTR operated at HRT=12 h under steady-
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55 107 state at the lab. This inoculum had been characterized by pyrosequencing in
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57 108 previous work ([Bakonyi et al., 2017](#)), finding the dominance of **hydrogen-producing**
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4 109 microorganisms such as *Clostridium pasteurianum* and *Pectinatus frisingensis* in the
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7 110 microbial community.

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9 111 Adopting the sludge from the reactor used in the work of [Bakonyi et al.](#)
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11 112 ([2017](#)), two CSTRs were started-up in this work, differing in process HRT and
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14 113 corresponding OLR. In the two separate reactors (referred as Reactor 1 and 2
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17 114 onward), HRT of 6 h and 10 h were adjusted, respectively. Corresponding OLRs
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20 115 were 85.6 g COD/L-d and 51.4 g COD/L-d, employing glucose as a substrate in the
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23 116 culture medium at a constant concentration of 20 g/L (1.07 g COD/g glucose).
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25 117 Besides glucose, **as carbon source**, for every liter of feed solution, the following
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28 118 amounts of mineral salts – modified from [Ramírez-Morales et al. \(2015\)](#) – were
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31 119 supplied: K₂HPO₄, 50 mg; NH₄Cl, 104 mg; MnCl₂·4H₂O, 0.4 mg; MgCl₂·6H₂O, 20
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33 120 mg; FeSO₄·7H₂O, 20 mg; CoCl₂·6H₂O, 2 mg; Na₂MoO₄·2H₂O, 2 mg; H₃BO₄, 2 mg;
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35 121 NiCl₂·6H₂O, 2 mg; ZnCl₂, 2 mg. The media was prepared using tap water and
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38 122 refrigerated at 4 °C to minimize fluctuations in its composition.

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41 123 Both Reactors 1 and 2, had 1.25 L/0.9 L total/working volumes. First, the
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44 124 CSTRs **operated in batch mode** for 24 h with 10 g glucose/L at initial volatile
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47 125 suspended solid (VSS) concentration of 4 g/L. Afterward, the reactors were
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50 126 switched to continuous mode and the glucose concentration was increased to 20 g/L
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52 127 in the medium and maintained constant onward, as mentioned above. Steady-state
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54 128 was considered once stable H₂ production (± 10-15 % daily variation) could be
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57 129 reached at least for 2 consecutive days ([Lin et al., 2008](#)).

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4 130 The reactors were equipped with an EZ-Bioreactor Control device (Applikon
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7 131 Biotechnology, Schiedam, The Netherlands) and operated at 35 °C. 100 rpm stirring
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10 132 rate by an upper shaft agitator with 2 equally spaced Rushton turbines was ensured.
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12 133 The pH was maintained at 5.5 by 3M NaOH and 3M HCl solutions. A conductivity-
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15 134 based on/off level sensor was built-in to precisely control the liquid level. The
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17 135 scheme of the experimental apparatus was based on earlier work ([Ramírez-Morales](#)
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20 136 [et al. 2015](#)) and is shown in **Fig. 2**. Initially, the bioreactors were purged with >99.9
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23 137 % N₂ to establish fully anaerobic conditions.
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27 28 139 **2.2. Selection of conditions for perturbation tests (OLR, HRT)**

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33 141 The following experimental plan was executed to test reactor stability and
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36 142 robustness over time as a response to feeding perturbations. In both Reactor 1 and 2,
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38 143 shocking HRTs of 5 and 3 hours were applied, resulting in OLRs of 102.7 and 171.2
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41 144 g COD/L-d, respectively. The durations were varied either as 6 or 24 hours. These
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44 145 operating conditions were chosen according to the presented literature and previous
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47 146 results.

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49 147 Concerning the OLR selection, **Fig. 3** shows the hydrogen productivity at
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52 148 several OLR values tested by various authors. Accordingly, an OLR between 90 and
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55 149 120 g COD/L-d seems to foster the biohydrogen production. **Nonetheless**, above this
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57 150 **range** (>120 g COD/L-d), a disadvantageous effect can occur, depressing the H₂
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60 151 productivity. Hence, one perturbing OLR value (102.7 g COD/L-d) that falls to the
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152 90-120 g COD/L-d range has been selected, as well as one value that is out of such
153 range and likely disadvantageous (171.2 g COD/L-d).

154 Regarding the HRT and glucose input concentration selection, Ramírez-
155 Morales et al. (2015) reported maximum hydrogen productivity of 25.4 L H₂/L-d at
156 HRT=4 h and under an optimum value of OLR (100 g COD/L-d) given by a fixed
157 substrate concentration (16.7 g glucose/L). Moreover, Villa-Leyva (2015) found that
158 at 25 g glucose/L and 106.7 g COD/L-d (HRT=6 h), glucose consumption by the
159 biological system decreased from 97% to 81% due to substrate overload, using a
160 CSTR and the same type of sludge and inoculum pretreatment than in this research.

161 Furthermore, Valdez-Vazquez and Poggi-Varaldo (2009) documented the
162 specific growth rate for both hydrogen-producing bacteria (0.083 h⁻¹) and
163 methanogenic archaea (0.0167 h⁻¹), which diminish the hydrogen production. In this
164 sense, it was convenient to operate reactors at high dilution rates and hence low
165 HRT (around 12 h or even lower) to promote the washout of methanogenic archaea
166 and prevent their growth. These results were the basis for setting the experimental
167 conditions of this work (regarding shocking HRT and OLR) to even suboptimal
168 values to assess the H₂-producing capacity of either bioreactors or the biological
169 system.

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171 **2.3 Analytical methods**

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173 The composition of biogas samples (hydrogen, carbon dioxide and methane
174 contents) was determined by gas chromatography (SRI Model 8610c) using thermal
175 conductivity detector. The analysis of volatile fatty acids – acetic acid (HAc),
176 butyric acid (HBu) – was performed on a gas chromatograph (Agilent technologies
177 model 7890B) connected to a flame ionization detector. Both methodologies were
178 followed as described by [Buitrón and Carvajal \(2010\)](#). The volume of biogas
179 produced was measured by a MilliGascounter (Ritter, Germany) connected to the
180 COM1 serial port of a desk computer (PC). Glucose consumption was followed by
181 the phenol/sulfuric acid method ([DuBois et al. 1956](#)).

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183 **2.4 Calculations**

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185 H₂ productivity was calculated according to Eq. 1:

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$$P_{H_2} = V_H / (V_R t) \tag{1}$$

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189 where P_{H₂} is the H₂ productivity (L H₂/L-d), V_H is the volume of H₂ produced (L),
190 V_R is the reactor working volume (L) and t is the operational time or sampling time
191 for each H₂ volume measurement. Volumes of H₂ are referred to Standard

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4 192 Temperature and Pressure (STP) conditions (273.15 K and 100 kPa, respectively).
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7 193 **On the other hand, H₂ yield was calculated according to Eq. 2:**
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$$Y_{H_2} = n_H/n_G \quad (2)$$

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17 197 where n_H and n_G are the amounts of hydrogen produced (mol) and glucose
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20 198 consumed (mol), respectively.
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25 200 **2.5 Statistical evaluation**
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31 202 A statistical approach was applied to assess the impact of process
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33 203 perturbations caused by feeding shocks (both the shocking HRT and its duration) on
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36 204 the hydrogen production rate (HPR) **regarding the statistically significant difference.**
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39 205 This approach consisted of performing a two-way analysis of variance (ANOVA) to
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41 206 the whole H₂ productivity data for each reactor separately with the aim of finding
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44 207 any statistical difference between either HRT or **the feeding shock** duration on the
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47 208 HPR.
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49 209 In this sense, Bartlett test was also applied to check the homogeneity of
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52 210 variances in each group of data. This test consists of statistical analysis about a
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55 211 variance to find out if variances **among** the experimental treatments are equal or not.
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57 212 The Bartlett statistic allows accepting the hypothesis of equal variances among the
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213 different levels of a variable when it is below or equal to $X^2_{\alpha;\alpha-1}$. The statistical
214 analysis was conducted using R software.

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216 **3. Results and Discussion**

217 **3.1 Performance of continuous hydrogen producing bioreactors under non-** 218 **disturbed and shocking conditions**

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220 In Reactor 1 (operated at HRT=6 h, OLR=85.6 g COD/L-d), steady-state was
221 reached after 2 days operation, achieving average hydrogen productivity of 17.3 L
222 H₂/L-d. Then, the reactor was subjected to four organic shock loads (two at HRT=5
223 h, OLR=102.7 g COD/L-d during 6 and 24 hours respectively, and two at HRT=3 h,
224 OLR=171.2 g COD/L-d with the same duration), as shown in **Fig. 4**. It is important
225 to note that no substantial increase in the hydrogen productivity could be observed
226 **after the four temporary feeding shocks**, as illustrated in **Fig. 4**. Also, this set of
227 experiments with Reactor 1 evidenced the robustness of **both** the biological system
228 **and** reactor to withstand HRTs even as low as 3 hours for the **tested** period.

229 Considering those preliminary results, Reactor 2 (operated at HRT=10h,
230 OLR=51.4 g COD/L-d) was perturbed with 5 and 3 hours of shocking HRT to cause
231 higher (more intense) organic loading increases (102.7 and 171.2 g COD/L-d
232 respectively) and evaluate the reactor robustness in such case. Once again, two
233 different durations of the shocking HRT were assessed (6 and 24 hours). **In this**
234 **context, Fig. 5** shows the associated results, where it can be observed that mean H₂

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235 productivity of 12.4 L H₂/L-d was achieved during the steady state (non-disturbed
236 operation), given by the values represented by blue dots in **Fig. 5**, which was much
237 lower than in Reactor 1 (17.3 L H₂/L-d).

238 Besides, it **was observed** from the outcomes that an increase in the organic
239 loading **rate leads** the biological system towards the **enhancement of the** hydrogen
240 production. It is noteworthy that regardless of which reactor is considered, the H₂
241 production performance was successfully recovered after each HRT/OLR
242 perturbation, meaning that similar steady-state HPRs could be noted before and after
243 each temporary introduced shock. The statistical analysis supported such behavior.

244 In this sense, two-way ANOVA was performed on the hydrogen productivity
245 data of each reactor (Table 1), whose results revealed that both HRT (p-value=8x10⁻
246 ⁴) and shocking duration (p-value=1.2x10⁻³) had a significant statistical impact on
247 the H₂ productivity in Reactor 2 operated at HRT=10 h. That **evidence the**
248 **significant effect of the feeding shocks on the HPR in a scenario where the shocking**
249 **HRT substantially different from the operating HRT.**

250 Concerning Reactor 1 and examining **Fig. 4**, it seems that neither the
251 shocking HRT nor its duration had a significant effect on the HPR. The ANOVA
252 confirms the results (Table 1, p-values of 0.967 and 0.327 respectively).
253 Nevertheless, the interaction between both variables did have a statistically
254 significant effect on the H₂ productivity (p-value=0.016) in Reactor 1, operated at
255 HRT= 6 h, which could not be simply observed from **Fig. 4**.

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256 Also, Bartlett test was executed to each reactor, which confirmed the
257 homogeneity of variances in all levels of the process variables (HRT and duration)
258 for both Reactors 1 and 2, given by p-values of 0.072 and 0.761 respectively (Table
259 1).

260 In conclusion, statistical results evidenced the increase in hydrogen
261 production under shocking HRT, mainly in Reactor 2 (HRT=10 h) due to the higher
262 difference between organic loads in this reactor in comparison to Reactor 1 operated
263 at HRT=6 h. Nevertheless, in the light of mean HPRs in Reactors 1 and 2, 40%
264 improvement was achieved in **Reactor 1**, which coincides with the common
265 literature finding that shorter process HRT/higher OLR may result beneficial
266 **regarding** hydrogen production. In particular, as it was **already** demonstrated,
267 shortening the HRT normally in the range of 12-6 h (until a threshold level where
268 wash out of useful **bacteria** could potentially occur) can enhance the H₂-formation
269 (Hawkes et al., 2002; Tapia-Venegas et al., 2013).

270 **Furthermore**, it is deduced that both systems are robust enough to endure the
271 process shocks applied in an equally promising way. That is in agreement with the
272 relevant literature, **considering the** similar robustness of a hydrogen-producing
273 fermenter. **Park et al. (2015)** demonstrated that despite the various harsh
274 disturbances subjected to the reactors (shock loading, acidification, starvation and
275 alkalization) caused temporary changes, the original performance and therefore, the
276 steady state could always be restored.

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277 According to the literature (**Fig. 3**), an OLR exceeding 120 g COD/L-d may
278 cause a process inhibition. Nevertheless, operating results presented in this research
279 using an OLRs of 171.2 g COD/L-d, (**Figs. 4 and 5**) demonstrated that the reactors
280 could be operated within this range (for a period up to 24 hours) without significant
281 washout, drop in the H₂ productivity and deterioration of reactor stability. Thus the
282 long-term reactor performance is not affected.

283

284 **3.2 Correlation of H₂ production efficiency with VFA patterns for the 10h-HRT** 285 **reactor**

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287 By correlating the results of volatile fatty acids (acetic and butyric acids)
288 analysis with H₂ production performance – for example as given in **Fig. 6A** for
289 Reactor 2, operated at 10 h of HRT – it is implied that the hydrogen evolution
290 (**expressed as HPR**) under non-disturbed conditions (**steady-state under HRT=10 h**)
291 was dependent on the butyric to the acetic acid ratio (HBu/HAc). In other words,
292 although only slight fluctuations of H₂ productivity were noted throughout the non-
293 disturbed state as mentioned before, these fluctuations were always accompanied by
294 **some** changes in the distribution of soluble metabolic products (HAc, HBu). Higher
295 HBu/HAc ratios reflected those changes **along the course of the process, which also**
296 **promoted better gas formation efficiency (Fig. 6A)**. Such behavior agrees with the
297 results of other literature studies communicating enhanced H₂ generation at higher
298 HBu/HAc ([Chen et al. 2002](#); [Kim et al. 2006](#)), which has been a routine parameter to

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299 judge the effectiveness of the system (Arooj et al. 2008). Moreover, it was shown
300 that butyrate-dominant metabolism in hydrogen-producing anaerobic cultures
301 utilizing glucose is thermodynamically favored (Lee et al. 2008).

302 Additionally, H₂ productivity had a direct relationship with hydrogen yield
303 (Fig. 6B), which could reach values as high as 60-70 % of the practical upper-bound
304 (4 mol H₂/mol glucose) (Hallenbeck, 2009). Moreover, Fig. 6C relates the hydrogen
305 yield against the H_{Bu}/H_{Ac} ratio revealing that in general high H_{Bu}/H_{Ac} ratios
306 foster high H₂ yields. The efficiencies found regarding H₂ yield have been typically
307 published for hydrogen-producing biosystems by dark fermentation with mixed
308 microbial consortia (Lee et al. 2010).

309 Finally, it could be noticed that the biogas compositions – irrespective of the
310 HRT – had no significant variations (60-63 vol.% H₂ and 37-40 vol.% CO₂) and
311 without methane detection. This stability in the gas composition is advantageous for
312 biohydrogen upgrading purposes using membrane technology (Bakonyi et al. 2015,
313 2016). Such improving method has been shown as a promising downstream
314 technology for the purification and concentration of H₂ (Bakonyi et al. 2013;
315 Ramírez-Morales et al. 2013; Shen et al. 2009) before feeding it to efficient fuel
316 cells for power generation.

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318 **4. Conclusions**

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320 The robustness of continuous biohydrogen fermenters to process disturbances
321 such as organic shock loads, with the concomitant HRT shocks, and **their** related
322 durations was examined. **It** turned out that CSTR reactors fairly withstand **the**
323 **feeding shocks. The results indicated that the H₂ productivity was statistically**
324 **significant (ANOVA) improved by the temporary organic shock loads, increasing**
325 **the HPR up to 40%. After the applied shocks the initial average H₂ productivity is**
326 **restored, irrespective of the shocks applied (3 and 5 hours of HRT, corresponding to**
327 **171.2 and 102.7 g COD/L-d of OLR respectively, lasting either 6 or 24 hours).**
328 **The outcomes presented in this research indicate that hydrogen-producing reactors**
329 **can be robust enough to withstand process shocks. Those results are useful to**
330 **develop a hydrogen productivity optimization strategy.**

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331 **References**

332

333 Arooj MF, Han SK, Kim SH, Kim DH, Shin HK (2008) Continuous biohydrogen
334 production in a CSTR using starch as a substrate. *Int J Hydrogen Energy* 33:3289-
335 3294. <http://dx.doi.org/10.1016/j.ijhydene.2008.04.022>

336 Baghchehsaraee B, Nakhla G, Karamanev D, Margaritis A (2011) Revivability of
337 fermentative hydrogen producing bioreactors. *Int J Hydrogen Energy* 36:2086-2092.
338 <http://dx.doi.org/10.1016/j.ijhydene.2010.11.038>

339 Bakonyi P, Bogdán F, Kocsi V, Nemestóthy N, Bélafi-Bakó K, Buitrón G (2016)
340 Investigating the effect of hydrogen sulfide impurities on the separation of
341 fermentatively produced hydrogen by PDMS membrane. *Sep Purif Technol*
342 157:222-228. <http://dx.doi.org/10.1016/j.seppur.2015.11.016>

343 Bakonyi P, Buitrón G, Valdez-Vazquez I, Nemestóthy N, Bélafi-Bakó K (2017) A
344 novel gas separation integrated membrane reactor to evaluate the impact of self-
345 generated biogas recycling on continuous hydrogen fermentation. *Appl Energy*
346 190:813-823. <http://dx.doi.org/10.1016/j.apenergy.2016.12.151>

347 Bakonyi P, Nemestóthy N, Bélafi-Bakó K (2013) Biohydrogen purification by
348 membranes: An overview on the operational conditions affecting the performance of
349 non-porous, polymeric and ionic liquid based gas separation membranes. *Int J*
350 *Hydrogen Energy* 38:9673-9687. <http://dx.doi.org/10.1016/j.ijhydene.2013.05.158>

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351 Bakonyi P, Nemestóthy N, Lankó J, Rivera I, Buitrón G, Bélafi-Bakó K (2015)
352 Simultaneous biohydrogen production and purification in a double-membrane
353 bioreactor system. Int J Hydrogen Energy 40:1690-1697.
354 <http://dx.doi.org/10.1016/j.ijhydene.2014.12.002>

355 Bakonyi P, Nemestóthy N, Simon V, Bélafi-Bakó K (2014) Fermentative hydrogen
356 production in anaerobic membrane bioreactors: A review. Bioresour Technol
357 156:357-363. <http://dx.doi.org/10.1016/j.biortech.2014.01.079>

358 Bakonyi P, Nemestóthy N, Simon V, Bélafi-Bakó K (2014) Review on the start-up
359 experiences of continuous fermentative hydrogen producing bioreactors. Renew
360 Sustain Energy Rev 40:806-813. <http://dx.doi.org/10.1016/j.rser.2014.08.014>

361 Buitrón G, Carvajal C (2010) Biohydrogen production from Tequila vinasses in an
362 anaerobic sequencing batch reactor: Effect of initial substrate concentration,
363 temperature and hydraulic retention time. Bioresour Technol 101:9071-9077.
364 <http://dx.doi.org/10.1016/j.biortech.2010.06.127>

365 Buitrón G, Kumar G, Martinez-Arce A, Moreno G (2014) Hydrogen and methane
366 production via a two-stage processes (H₂-SBR + CH₄-UASB) using tequila vinasses.
367 Int J Hydrogen Energy 39:19249-19255.
368 <http://dx.doi.org/10.1016/j.ijhydene.2014.04.139>

369 Chen CC, Lin CY, Lin MC (2002) Acid-base enrichment enhances anaerobic
370 hydrogen production process. Appl Microbiol Biotechnol 58:224-228.
371 <http://dx.doi.org/10.1007/s002530100814>

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64
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372 DuBois M, Gilles KA, Hamilton JK, Rebers PA, Smith F (1956) Colorimetric
373 method for determination of sugars and related substances. Anal Chem 28:350-356.
374 <http://dx.doi.org/10.1021/ac60111a017>

375 Hafez H, Nakhla G, Naggar MHE, Elbeshbishy E, Baghchehsaraee B (2010) Effect
376 of organic loading on a novel hydrogen bioreactor. Int J Hydrogen Energy 35:81-92.
377 <http://dx.doi.org/10.1016/j.ijhydene.2009.10.051>

378 Hallenbeck PC (2009) Fermentative hydrogen production: Principles, progress, and
379 prognosis. Int J Hydrogen Energy 34:7379-7389.
380 <http://dx.doi.org/10.1016/j.ijhydene.2008.12.080>

381 Hawkes FR, Dinsdale R, Hawkes DL, Hussy I (2002) Sustainable fermentative
382 hydrogen production: challenges for process optimization. Int J Hydrogen Energy
383 27:1339-1347. [http://dx.doi.org/10.1016/S0360-3199\(02\)00090-3](http://dx.doi.org/10.1016/S0360-3199(02)00090-3)

384 Hernández-Mendoza CE, Buitrón G (2014) Suppression of methanogenic activity in
385 anaerobic granular biomass for hydrogen production. J Chem Technol Biotechnol
386 89:143-149. <http://dx.doi.org/10.1002/jctb.4143>

387 Hernández-Mendoza CE, Moreno-Andrade I, Buitrón G (2014) Comparison of
388 hydrogen-producing bacterial communities adapted in continuous and discontinuous
389 reactors. Int J Hydrogen Energy 39:14234-14239.
390 <http://dx.doi.org/10.1016/j.ijhydene.2014.01.014>

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391 Jung KW, Kim DH, Kim SH, Shin HK (2011) Bioreactor design for continuous dark
392 fermentative hydrogen production. *Bioresour Technol* 102:8612-8620.
393 <http://dx.doi.org/10.1016/j.biortech.2011.03.056>

394 Kim DH, Han SK, Kim SH, Shin HK (2006) Effect of gas sparging on continuous
395 fermentative hydrogen production. *Int J Hydrogen Energy* 31:2158-2169.
396 <http://dx.doi.org/10.1016/j.ijhydene.2006.02.012>

397 Krupp M, Widmann R (2009) Biohydrogen production by dark fermentation:
398 Experiences of continuous operation in large lab scale. *Int J Hydrogen Energy*
399 34:4509-4516. <http://dx.doi.org/10.1016/j.ijhydene.2008.10.043>

400 Kumar G, Bakonyi P, Kobayashi T, Xu KQ, Sivagurunathan P, Kim SH, Buitrón G,
401 Nemestóthy N, Bélafi-Bakó K (2016) Enhancement of biofuel production via
402 microbial augmentation: The case of dark fermentative hydrogen. *Renew Sustain*
403 *Energy Rev* 57:879-891. <http://dx.doi.org/10.1016/j.rser.2015.12.107>

404 Kumar G, Bakonyi P, Periyasamy S, Kim SH, Nemestóthy N, Bélafi-Bakó K (2015)
405 Lignocellulose biohydrogen: Practical challenges and recent progress. *Renew*
406 *Sustain Energy Rev* 44:728-737. <http://dx.doi.org/10.1016/j.rser.2015.01.042>

407 Lee HS, Salerno MB, Rittmann BE (2008) Thermodynamic evaluation on H₂
408 production in glucose fermentation. *Environ Sci Technol* 42:2401-2407.
409 <http://dx.doi.org/10.1021/es702610v>

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410 Lee HS, Vermaas WFJ, Rittmann BE (2010) Biological hydrogen production:
411 prospects and challenges. Trends Biotechnol 28:262-271.
412 <http://dx.doi.org/10.1016/j.tibtech.2010.01.007>

413 Lin CY, Chang CC, Hung CH (2008) Fermentative hydrogen production from starch
414 using natural mixed cultures. Int J Hydrogen Energy 33:2445-2453.
415 <http://dx.doi.org/10.1016/j.ijhydene.2008.02.069>

416 Park JH, Kumar G, Park JH, Park HD, Kim SH (2015) Changes in performance and
417 bacterial communities in response to various disturbances in a high-rate biohydrogen
418 reactor fed with galactose. Bioresour Technol 188:109-116.
419 <http://dx.doi.org/10.1016/j.biortech.2015.01.107>

420 Ramírez-Morales JE, Tapia-Venegas E, Nemestóthy N, Bakonyi P, Bélafi-Bakó K,
421 Ruiz-Filippi G (2013) Evaluation of two gas membrane modules for fermentative
422 hydrogen separation. Int. J. Hydrogen Energy 38:14042-14052.
423 <http://dx.doi.org/10.1016/j.biortech.2015.01.107>

424 Ramírez-Morales JE, Torres Zúñiga I, Buitrón G (2015) On-line heuristic
425 optimization strategy to maximize the hydrogen production rate in a continuous
426 stirred tank reactor. Process Biochem 50:893-900.
427 <http://dx.doi.org/10.1016/j.procbio.2015.03.003>

428 Shen L, Bagley DM, Liss SN (2009) Effect of organic loading rate on fermentative
429 hydrogen production from continuous stirred tank and membrane bioreactors. Int J
430 Hydrogen Energy 34:3689-3696. <http://dx.doi.org/10.1016/j.ijhydene.2009.03.006>

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64
65

431 Show KY, Lee DJ, Chang JS (2011) Bioreactor and process design for biohydrogen
432 production. *Bioresour Technol* 102:8524-8533.
433 <http://dx.doi.org/10.1016/j.biortech.2011.04.055>

434 Sivagurunathan P, Kumar G, Bakonyi P, Kim SH, Kobayashi T, Xu KQ, Lakner G,
435 Tóth G, Nemestóthy N, Bélafi-Bakó K (2016) A critical review on issues and
436 overcoming strategies for the enhancement of dark fermentative hydrogen
437 production in continuous systems. *Int J Hydrogen Energy* 41:3820-3836.
438 <http://dx.doi.org/10.1016/j.ijhydene.2015.12.081>

439 Tapia-Venegas E, Ramirez JE, Donoso-Bravo A, Jorquera L, Steyer JP, Ruiz-Filippi
440 G (2013) Bio-hydrogen production during acidogenic fermentation in a multistage
441 stirred tank reactor. *Int J Hydrogen Energy* 38:2185-2190.
442 <http://dx.doi.org/10.1016/j.ijhydene.2012.11.077>

443 Thanwised P, Wirojanagud W, Reungsang A (2012) Effect of hydraulic retention
444 time on hydrogen production and chemical oxygen demand removal from tapioca
445 wastewater using anaerobic mixed cultures in anaerobic baffled reactor (ABR). *Int J*
446 *Hydrog Energy* 37:15503-15510. <http://dx.doi.org/10.1016/j.ijhydene.2012.02.068>

447 Valdez-Vazquez I, Poggi-Varaldo HM (2009) Hydrogen production by fermentative
448 consortia. *Renew Sustain Energy Rev* 13:1000-1013.
449 <http://dx.doi.org/10.1016/j.rser.2008.03.003>

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60
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64
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450 Villa-Leyva A (2015) Optimización heurística de un fermentador productor de
451 hidrógeno modificando la carga orgánica. UNIVERSIDAD NACIONAL
452 AUTÓNOMA DE MÉXICO, MÉXICO, D. F.

453 Wang J, Wang W (2009) Factors influencing fermentative hydrogen production: A
454 review. Int J Hydrogen Energy 34:799-811.
455 <http://dx.doi.org/10.1016/j.ijhydene.2008.11.015>

456 Zhang A (2014) Real Time Optimization of Hydrogen Production in a Continuous
457 Fermentation Bioreactor. Institute of Chemical Technology, Prague.
458 [https://lib.ugent.be/fulltxt/RUG01/002/166/586/RUG01-
459 002166586_2014_0001_AC.pdf](https://lib.ugent.be/fulltxt/RUG01/002/166/586/RUG01-002166586_2014_0001_AC.pdf)

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10 464 **Fig. 1** Potential difference between laboratory and real-case fermentation conditions
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12 465 **Fig. 2** Experimental continuous hydrogen production system used by Ramírez-
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14 Morales et al. (2015)
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17 467 **Fig. 3** Comparison of literature studies regarding the effect of OLR on H₂
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19 productivity.
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22 469 **Fig. 4** Hydrogen productivity and Organic Loading Rate in Reactor 1 operated at
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24 HRT=6h subjected to two feeding shocks of 102.7 g COD/L-d (HRT=5h) and two
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26 shocks of 171.2 g COD/L-d (HRT=3h)
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30 472 **Fig. 5** Hydrogen productivity and Organic Loading Rate in Reactor 2 operated at
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32 HRT=10h subjected to two feeding shocks of 102.7 g COD/L-d (HRT=5h) and two
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34 shocks of 171.2 g COD/L-d (HRT=3h)
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38 475 **Fig. 6** (A) The dependency of H₂ production performance on butyric to acetic acid
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40 ratio (HBu/Hac), (B) The correlation of H₂ productivity with H₂ yield and (C) The
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42 relationship between hydrogen yield and HBu/Hac ratio under non-disturbed
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45 conditions in a CSTR operated with process HRT of 10 h.
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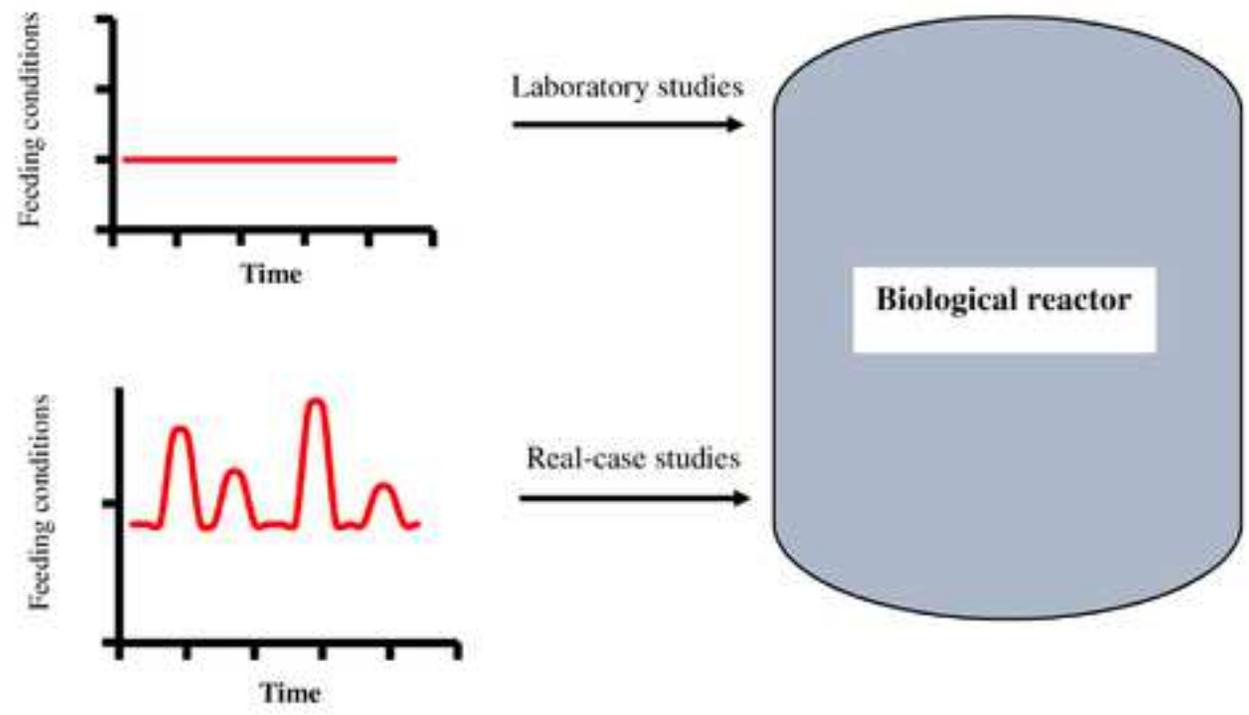
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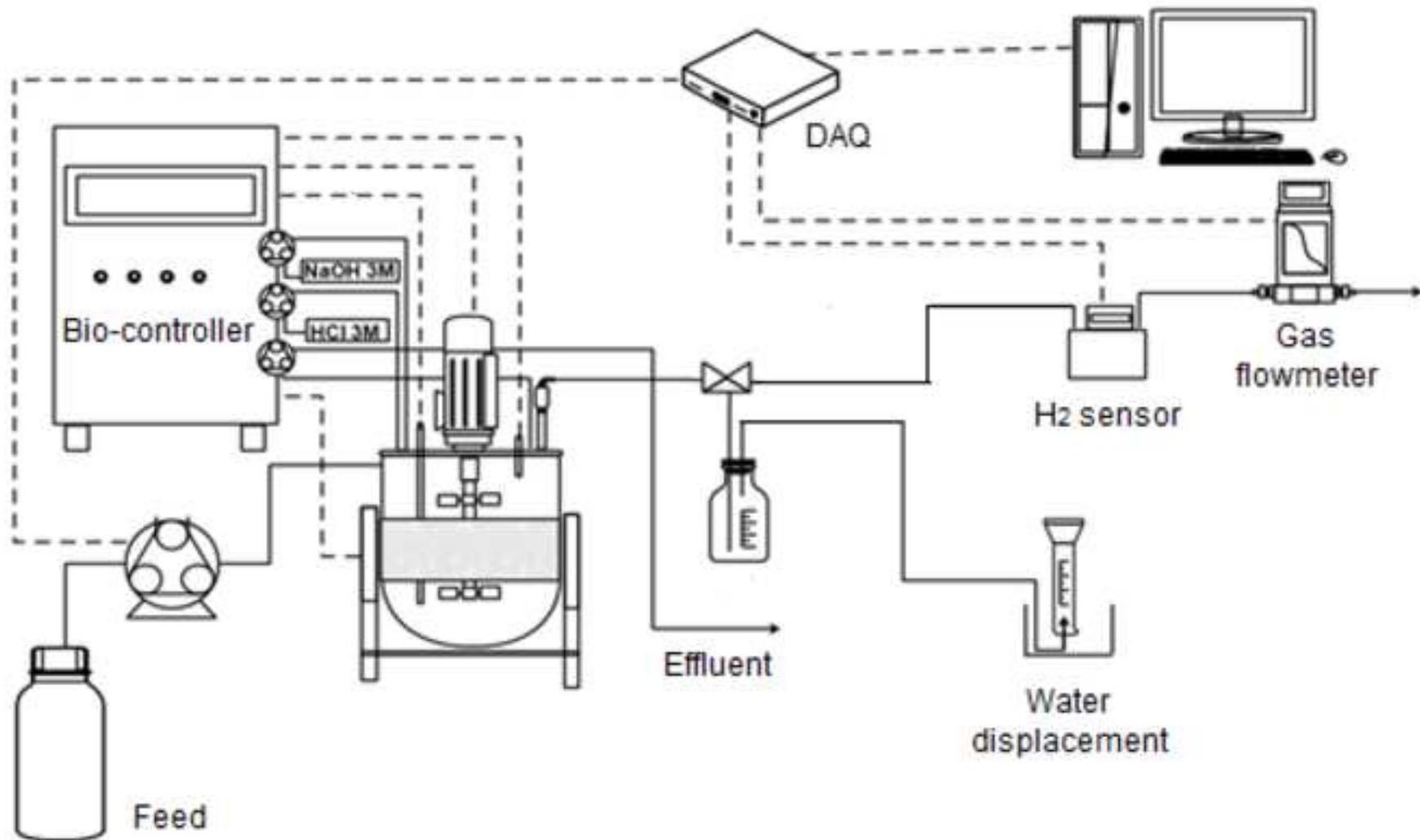
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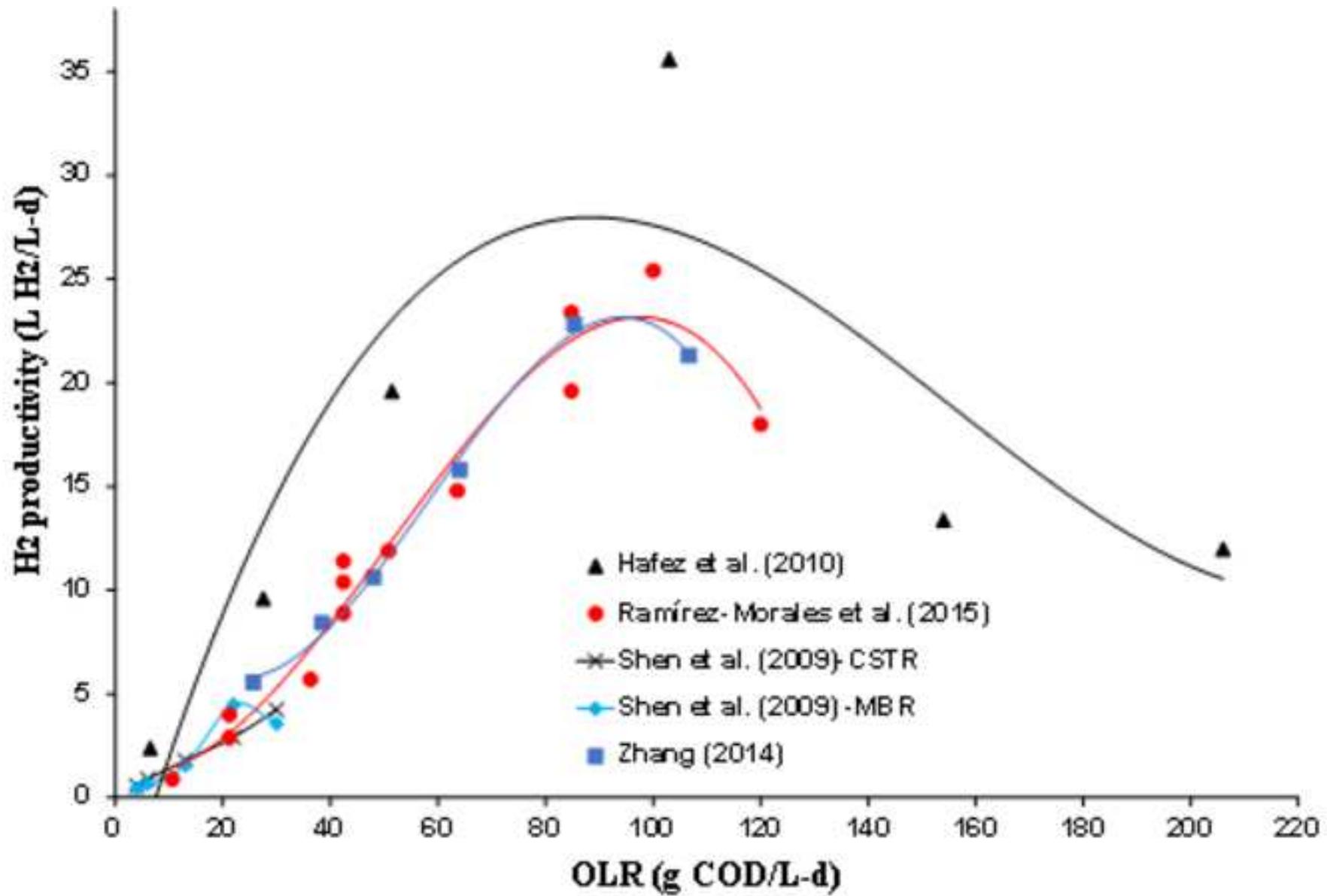
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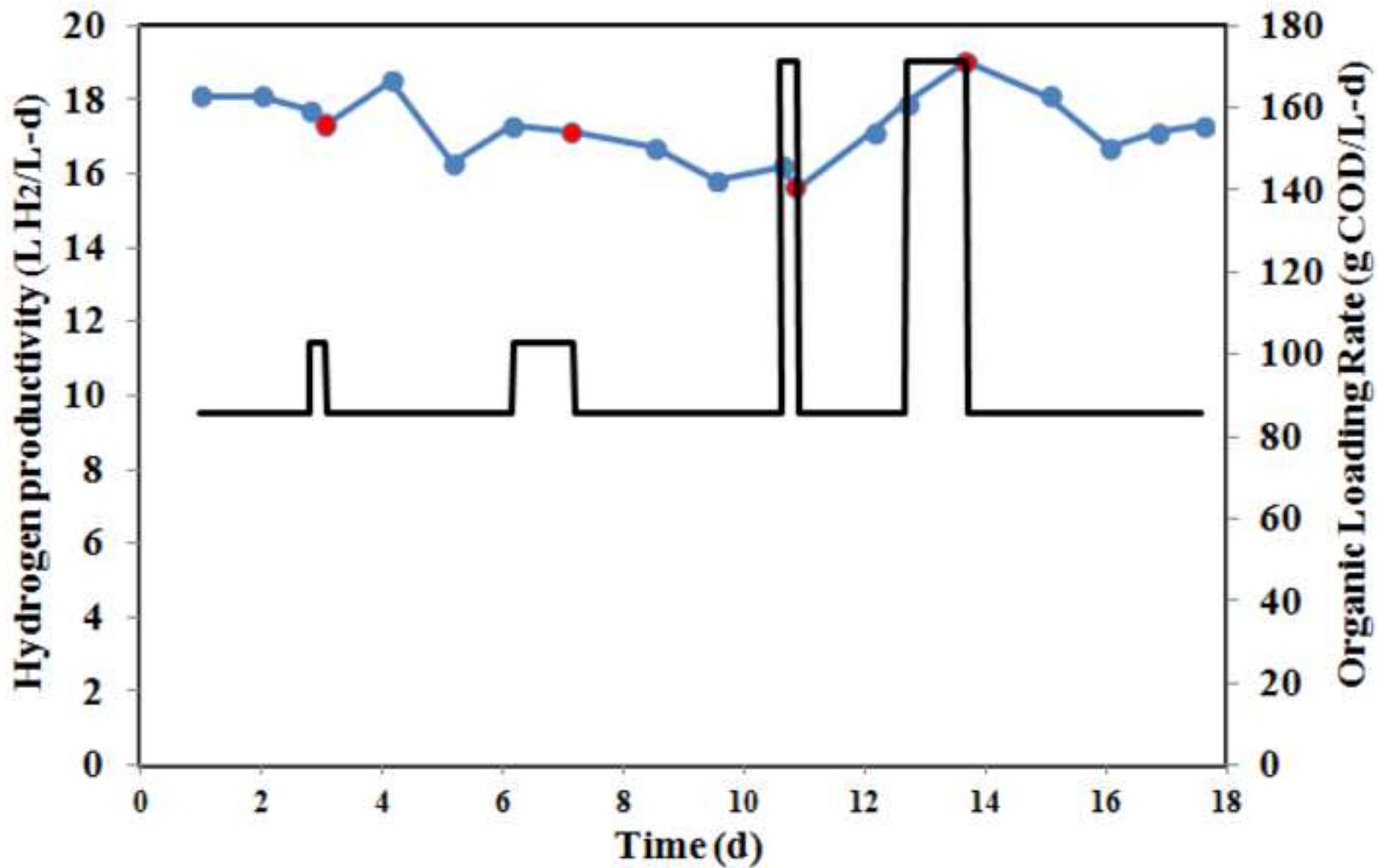
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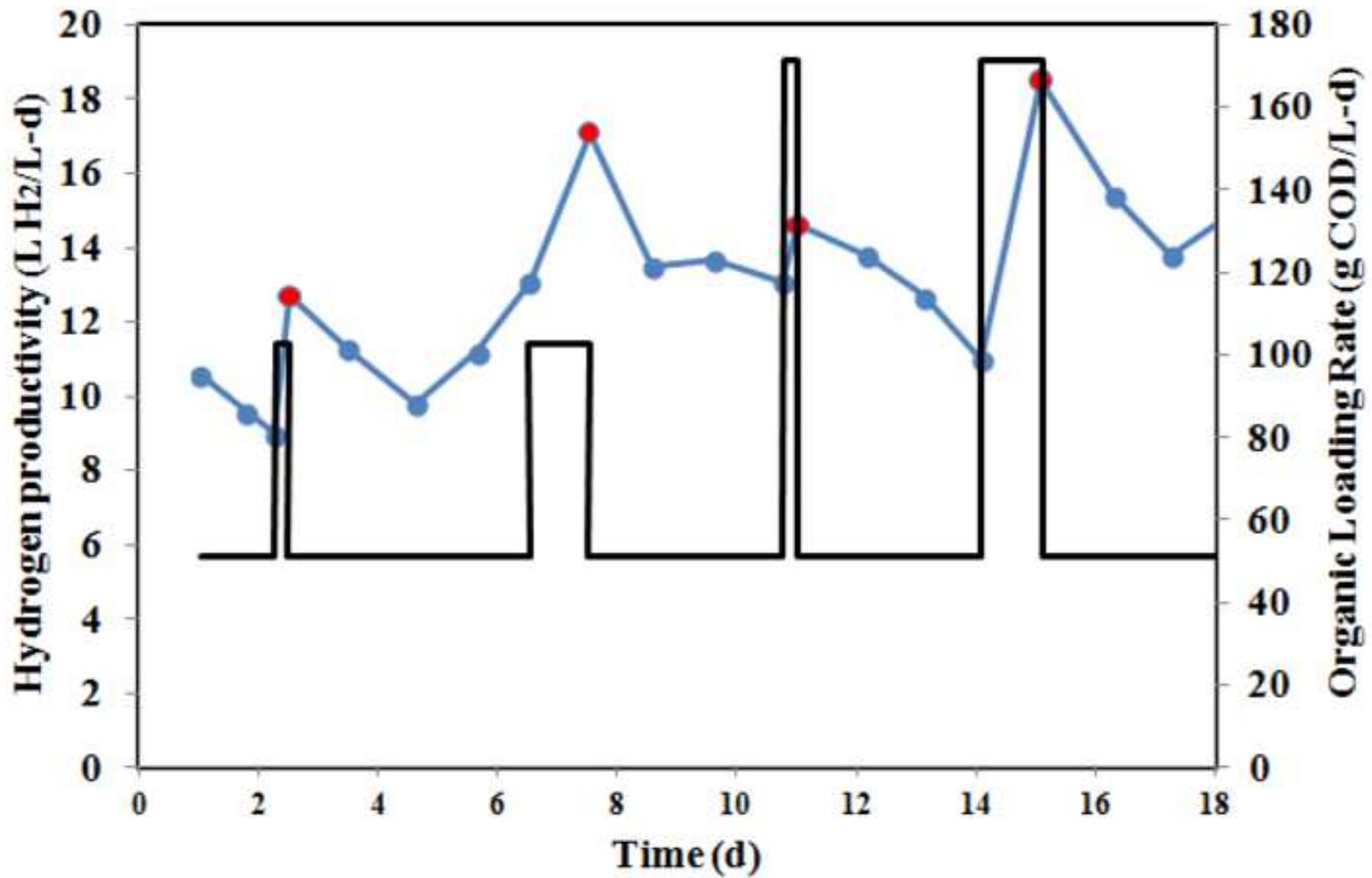
481 **Table 1.** Bartlett test and two-way ANOVA results on the significance of HRT and
482 feeding shocks duration on the bioreactor performance











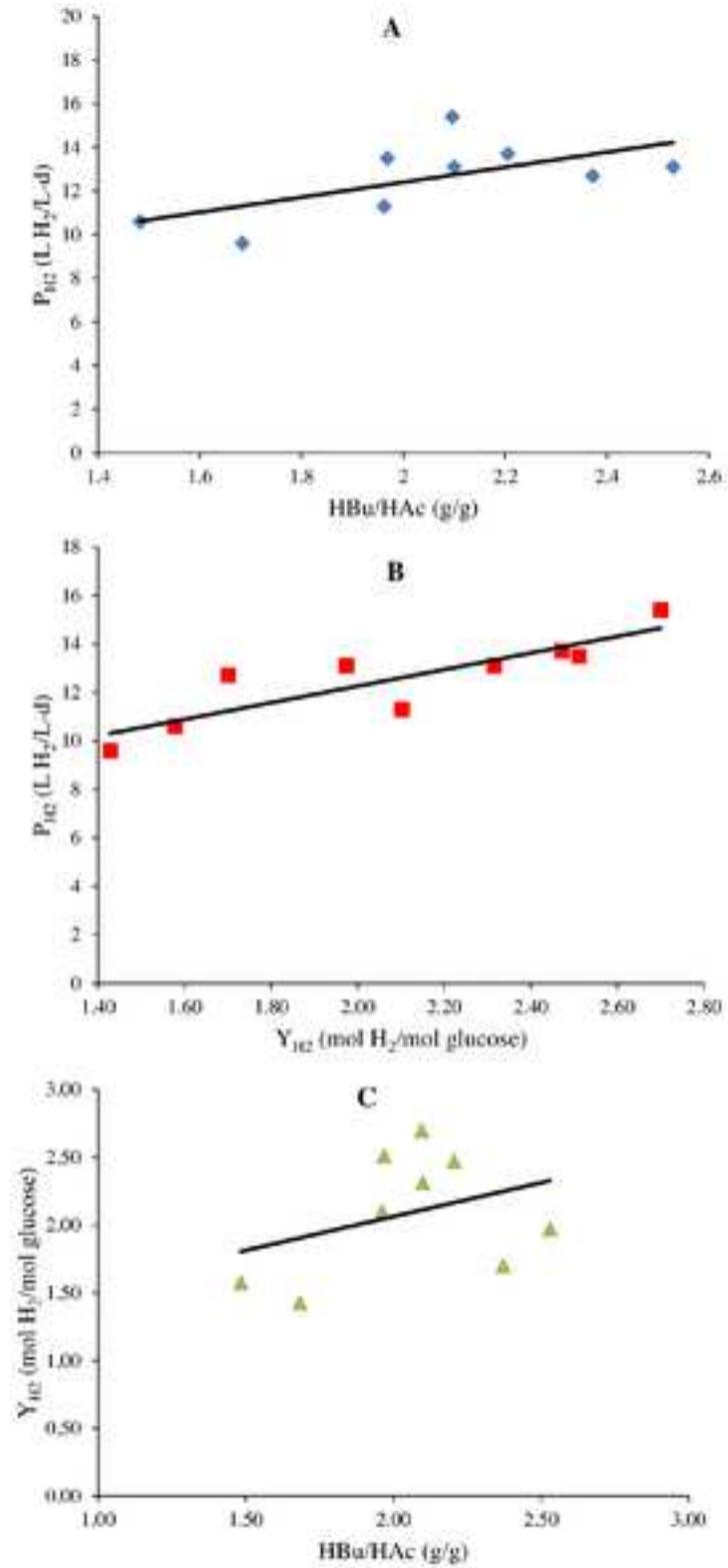


Table 1

Reactor 1				Reactor 2				
HRT (h)	Duration (h)	P _{H2} (L H ₂ /L-d)	Y _{H2} (mol H ₂ /mol glucose)	HRT (h)	Duration (h)	HBu/HAc (g/g)	P _{H2} (L H ₂ /L-d)	Y _{H2} (mol H ₂ /mol glucose)
6	24	18.1	1.82	10	25	1.48	10.6	1.58
6	24	18.1	1.94	10	18.3	1.68	9.6	1.43
6	19.6	17.7	1.88	10	11.4		9	1.34
5	6	17.3	1.29	5	6		12.7	1.06
6	26.2	18.5	1.86	10	23	1.96	11.3	2.10
6	24	16.3	1.64	10	27.5		9.8	1.82
6	24	17.3	1.78	10	25		11.2	2.04
5	24	17.1	1.45	10	20.6	2.10	13.1	2.31
6	32.7	16.7	1.58	5	24		17.1	1.59
6	24	15.8	1.59	10	25	1.97	13.5	2.51
6	26.2	16.2	1.63	10	25	2.20	13.7	2.47
3	6	15.6	0.80	10	27.5	2.53	13.1	1.97
6	30.5	17.1	1.37	3	6		14.6	0.81
6	13	17.9	1.92	10	27.5		13.8	2.57
3	24	19	0.95	10	23	2.37	12.7	1.70
6	32.7	18.1	1.88	10	23		11	2.05
6	24	16.7	1.29	3	24		18.5	0.98
6	19.6	17.1	1.60	10	29.7	2.10	15.4	2.70
6	17.5	17.3	1.68	10	23		13.8	2.49
				10	25		15	2.37

ANOVA RESULTS (based on P_{H2})

Variables (Reactor 1)	p-value	Variables (Reactor 2)	p-value
HRT	0.967	HRT	0.0008
Duration	0.327	Duration	0.0012
HRT:duration	0.016	HRT:duration	0.7798
Bartlett test	0.072	Bartlett test	0.7606

p<0.05 is considered statistically significant