

EXPERIMENTAL INVESTIGATION ON OPERATION PARAMETERS OF 3Å MOLECULAR SIEVE DESICCANT COATED TOTAL ENERGY RECOVERY WHEEL FOR MAXIMUM EFFECTIVENESS

by

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Original scientific paper
<https://doi.org/10.2298/TSCI180927012K>

The object of this research study was to investigate the maximum effectiveness values of the energy wheel by experimental tests conducted under extreme difference ambient air conditions parameters, different air volume flow rates, and energy wheel rotation speeds. Air temperature and humidity experimental tests were performed using a test facility that was developed and installed into the Indoor Air Quality and Thermal Comfort Laboratory of Budapest University of Technology and Economics. Our objective was to get the effectiveness values of sorption coated air-to-air energy recovery wheel for steady-state conditions under different ambient air (as supply air inlet) conditions. It was found that the sensible effectiveness increases by decreasing the volumetric flow rate through the wheel, and the optimum values of the effectiveness were given at the maximum wheel rotation speed based on the tests. As for the latent and total effectivenesses, their characteristics show an increasing trend by decreasing the air volume flow rate, ambient air temperature and relative humidity and increasing the wheel rotation speed.

Key words: *energy wheel, energy recovery, air handling unit, effectiveness, operation parameters, wheel rotation speed*

Introduction

The use of energy recovery units incorporated in Air Handling Units in commercial buildings increased significantly in the last 10 years. Rapid enhancement of energy efficiency is essential for a reduction in energy use and promotion of sustainable environment. Accordingly, improving energy performance of the building will significantly reduce the energy consumption [1-3]. Investments in these units are feasible, as it reduces the operating costs and improve more the energy efficiency [4, 5].

Energy recovery units, like the energy wheel, can be implemented in the design to transfer the indoor temperature and humidity (energy) to the incoming outdoor air. Therefore, more outdoor air can be used at a lower energy cost [6-8]. The exchange of indoor air for outdoor air represents a considerable wastage of energy, especially places, which need a higher rate of the air change per hour. Total energy recovery wheels transfer both sensible heat and moisture. In cooling mode, the outdoor air is precooled and dehumidified. In heating mode, the transfer of heat and moisture is reversed, as the outdoor air is preheated and pre-humidified [9, 10]. There are many advantages for applying the energy wheel as an energy recovery that

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includes simultaneous heat and mass transfer, low pressure drop, and available to all ventilation system platforms. The disadvantages of the energy wheel application are further cooling/heating required for supply air, there is possibility of cross-contamination, and it increases maintenance requirements especially under cold climates [11-14].

Previous work by researchers was highlighted in the literature review in order to specify the progress and development on energy recovery wheels.

Simonson and Besant [15] developed a numerical sample in rotating energy wheels and were calculated using the experimental data acquired. The performance of energy wheel was presented for a desiccant coating with a sorption isotherm (molecular sieve) and a linear sorption isotherm (silica gel). The numerical algorithm is changed from sorption to saturation when the air relative humidity exceeds 100% and when the wheel speed reduced the uncontrolled condensation and frosting reduced.

Experimental investigation had been executed by Sparrow *et al.* [16] to determine the operating conditions of an energy wheel. The sensible and moisture transfer effectiveness of a wheel device had been measured in a particular experimental facility. They found that the sensible effectiveness decreases by increasing the air volume flow rate and when the flow rates were matchless, higher values of effectiveness were came across. As for the moisture transfer effectiveness, the characteristic trend decreased by increasing flow rate.

Jeong and Mumma [17] developed practical effectiveness correlations for desiccant wheel. During their research linear equations were developed to calculate the desiccant wheel total effectiveness at nominal operating wheel speeds. The silica gel and molecular sieve coated wheel were investigated depending on six factors: outside air and temperature of exhaust air, relative humidity, air velocity, and air volume flow rate. It was found that the air velocity and air volume flow rate contribute highly to sensible and latent effectiveness. The entering outside air and exhaust air showed a small contribution to sensible effectiveness, and higher contribution to latent effectiveness.

Harmati *et al.* [18] analyzed the annual energy performance of office building located in the center of Belgrade to evaluate the energy recovery units in order to perform the most suitable heating and cooling solution.

Experimental investigations on desiccant wheel material was performed by Angrisani *et al.* [19] The results obtained by the authors were used to calculate the performance parameters as a function of the regenerated temperature, the inlet humidity ratio and the ratio between the regeneration and process air-flow rates. The obtained results indicated that the dehumidification process has a high influences on desiccant wheel material. It is because of the regeneration temperature instead of the regeneration air volume flow rate. The difference between the data was lower than 17%. Moreover, the maximum difference was less than about 20%. Low values of the RMSE have been accomplished as well.

In literature, no work was found to investigate the effectiveness of air-to-air energy recovery wheel coated with 3Å molecular sorption sieve under extreme difference ambient air conditions. No research results were found how the different air volume flow rates and different wheel rotation speeds as significant operation parameters influences the value of the sensible, latent and total effectivenesses. In this research work scientific experimental investigation was performed on the effect of different wheel rotation speeds on effectivenesses of sorption wheel under difference ambient air conditions and air volume flow rates. Optimal operating conditions are significantly important to know to reach the highest energy savings during different seasons. These results can be useful not only for researchers, developers, but also for building service and energy engineers in practice.

Description of the test facility

To achieve or research object an experimental test facility was installed into the Indoor Air Quality and Thermal Comfort Laboratory of Budapest University of Technology and Economics. The schematic diagram of the test facility is shown on fig. 1. A heat plate direct evaporation type exchanger used to generate the desired ambient air by a connected heat pump. Supply inlet air (as ambient air) was produced from the exhaust air flowing through the direct evaporator which cooled or heated up the air due to a refrigerator. Therefore, more extreme supply input air condition range with less energy demand can be established considering also the available cooling/heating capacity.

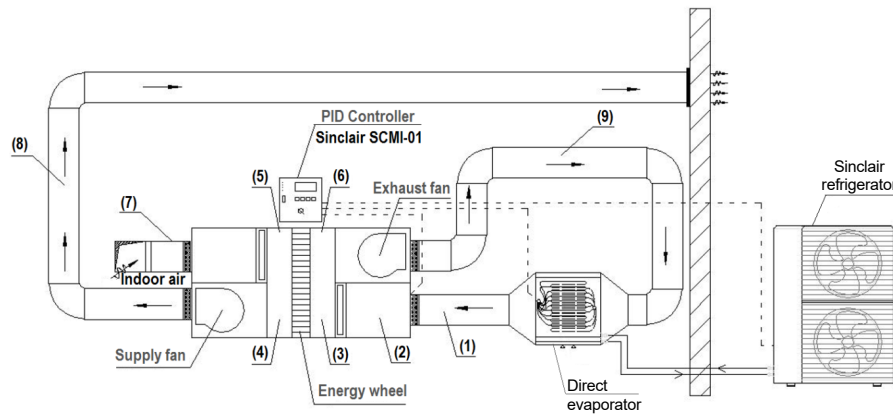


Figure 1. Schematic of the experimental test facility

Humidification of the supply and exhaust air was ensured by mist generators placed inside the air duct for the exhaust air and for the AHU sections for the supply air. The maximum capacity of evaporation unit was 1.8 Lph water for each one. Mist generators were placed into plastic trays. The generated mist adjusted and placed on a floating base while floating on top of the water inside the tray. However, due to their low capacities, the mist humidifiers were incorporated with ceramic water atomizer nozzles spraying water with rates of 12-20 Lph. This was fed by regulating tap water network pressure placed in points –9 as shown on fig. 1 to reach the desired and extreme relative humidity values.

Table 1 represents the path of air depending on to fig. 1 with the variable values measured at each point.

A high-efficiency Enventus [20] energy wheel was installed into the test facility, which transfers sensible energy (temperature) and latent energy (humidity) between the two air streams to recover the heat energy and provides proper air quality. The following specifications are given by the wheel producer in tab. 2.

Table 1. Variables measured on the experimental test facility

Point	Path of the air	Variables measured
1	Fresh air duct	$\dot{V}_{si} [m^3h^{-1}]$
2	AHU supply section	–
3	Sorption wheel (supply input)	$T_{si} [^{\circ}C], \phi_{si} [\%]$
4	Sorption wheel (supply output)	$T_{so} [^{\circ}C], \phi_{so} [\%]$
5	Sorption wheel (exhaust input)	$T_{ei} [^{\circ}C], \phi_{ei} [\%]$
6	Sorption wheel (exhaust output)	$T_{eo} [^{\circ}C], \phi_{eo} [\%]$
7	Indoor air duct	$\dot{V}_{ei} [m^3h^{-1}]$
8	Supply air duct	$\dot{V}_{so} [m^3h^{-1}]$
9	Exhaust air duct	$\dot{V}_{eo} [m^3h^{-1}]$

Table 2. Specifications of the investigated sorption wheel

Material of sorption wheel	Aluminum
Coating of sorption wheel	Molecular sieve 3
Coefficient of thermal conduction of the wheel	230 W/mK
Geometrical diameter of the wheel	540 mm
Geometrical width of the wheel	200 mm
Height of corrugated plates in the wheel	1.5 mm
Width of corrugated plates in the wheel	3 mm
Size of surfaces capable of heat-, and moisture transfer	170 m ²

Temperature, T_{si} , T_{so} , and T_{ei} , [°C], and relative humidity, φ_{si} , φ_{so} , and φ_{ei} [%], values were measured with the help of three Testo type humidity and temperature metering instruments, which were placed into the points as indicated on fig. 1. The calibration of these instruments was executed by the producer. These temperature and relative humidity measurements points which were located in the mid-plane of air ducts

before and after the energy wheel. The measurements were taken at the same time range to avoid fluctuation of supply side entering air temperature and exhaust side entering air temperature.

A Testo480 data recorder recorded the data measured by the metering devices. Intervals of 2 seconds were used. The Testo480 data was implemented to the PC through the producer application software. The volumetric flow rate of supply air was measured by another Testo hot-wire anemometer that was placed in the center of the air duct, at point – 8.

Experimental procedure

Experimental tests were conducted under different operating conditions to investigate the sensible, latent and total effectiveness of the sorption rotary wheel. The goal was to maintain the parameters measured constant as much as possible. Based on test measurements, the exhaust air inlet temperatures range during the test periods was set between $T_{ei} = 14\text{--}26$ °C and relative humidity range of $\varphi_{ei} = 25\text{--}55\%$.

Regulation of temperature and humidity of fresh air supplied

The supply air temperature, T_{si} , was set with the use of Sinclair SCMI-01 type PID controller as indicated in fig. 1 to regulate the power input in DC inverter refrigerator unit, installed to the test facility. The measurements were performed within the widest temperature and relative humidity possible range that the test facility can provide. As it could be regulated between the 10% to 100%, with 10%, intervals, the compressor begins to operate instead of the DC-Inverter compressor. The suitable selection of the P (proportional), I (integral), and D (derivative) parameters of the PID controller provided the minimization of the instability of the system. Therefore the proper PID parameter values were determined under different air conditions to obtain the desired temperatures with minimum fluctuations in the PID signals.

Relative humidity of supply input air, φ_{si} [%], was regulated with the help of ultrasound humidifiers placed into point – 2 as indicated in fig. 1. It was incorporated with two ceramic water atomizer nozzles spraying water that was placed into point – 9 to be able to obtain higher relative humidity range especially for higher volumetric flow rates. The ceramic insert spray nozzles were connected to the tap water network by pipes. The two water nozzles were separately connected to two water outlets. By this way there was no change on the water pressure that would influence the water spray rate.

Regulation of temperature and humidity of exhaust air

The temperature of exhaust air, T_{ei} [°C], was controlled with the use of a portable electrical air heater that was placed in point – 7 in fig. 2. The exhaust air, T_{ei} [°C], could only in-

crease the temperature to the desired range. The humidity of exhaust air, ϕ_{ei} [%], was regulated with the help of a two of the mentioned ultrasound humidifiers placed in point – 7 in fig. 1, that helped to increase the humidity to be $\phi_{ei} = 2-8\%$ by the turning on every ultrasound humidifier in separate.

Setting the speed of rotation of the wheel

The speed of rotation of the wheel, ω [rpm], was controlled with a potentiometer connected to the control panel. The speed of the wheel deducted from the voltage screen shown on the control panel. The speed-values were obtained through measurement, using a Voltcraft DT30LK type laser tachometer. Based on the results shown in tab. 3. wheel speed could be collected indirectly.

Table 3. Average wheel rotation speed ω [rpm] – voltage U [V] relation measurement

Average rotation speed [rpm]	Voltage [V]	Measurement duration [min]	Average fluctuation of rotation speed [\pm rpm]
1.998	0.83	10	0.002
6.059	2.87	10	0.002
10.030	4.80	10	0.002
15.088	7.28	10	0.002
20.011	9.69	10	0.002

Test plan

The measurement plan was compiled on the basis of the following aspects:

- The measurement plan was divided into two conditions (Summer and Winter).
- The indoor ambient conditions was selected as per recommended inside design values in ASHRAE HVAC Application as shown in tab. 4. [21]

Table 4. Recommended inside design conditions for summer and winter operations

Application	Summer				Winter		
	Extra		Commercial		With humidification		Without humidification
	T_{DB}	RH	T_{DB}	RH	T_{DB}	RH	T_{DB}
	[°C]	[%]	[°C]	[%]	[°C]	[%]	[°C]
Comfort house apartment	23-24	50-45	25-26	50-54	23-24	35-30	24-25
Retail shops	24-26	50-45	26-27	50-45	22-23	35-30	23-24
High latent load application	24-26	60-55	26-27	60-50	22-23	40-35	23-24
Factories	25-27	55-45	27-29	60-50	20-22	35-30	21-23

- From the tab. 4 the winter indoor conditions was selected to be as follows:

$$T_{ei} = 22 \text{ }^{\circ}\text{C}$$

$$\phi_{ei} = 35\%$$

While the summer indoor conditions was selected to be as follows:

$$T_{ei} = 24 \text{ }^{\circ}\text{C}$$

$$\phi_{ei} = 45\%$$

- The target values of fresh air temperature were conducted by a step of $T_{si} = 5^\circ\text{C}$ in the range of $T_{si} = -15$ to 0°C measured in winter conditions and $T_{si} = 5$ to 40°C measured in summer conditions.
- The target values of supply air inlet relative humidity were conducted by a step of $\phi_{si} = 10\%$ in the range of $\phi_{si} = 30$ to 100% measured in winter and summer. But the relative humidity of supply inlet air was 100% from $T_{si} = -15$ to 20°C .
- All target value pairs $T_{si} [^\circ\text{C}] - \phi_{si} [\%]$ were measured under different five rotational speeds.
- The input variable parameters for wheel speed was 2, 6, 10, 15, and 20 rpm.
- The input variable parameters for volume flow rate was 400, 600, 800, 1000, and 1200 m^3/h .
- All measurements were taken under continuous monitoring of the $T_{ei} [^\circ\text{C}]$, $\phi_{ei} [\%]$, \dot{V}_{so} [m^3/h] variables, and maintenance these values within the desired range.
- The order of setting wheel speed and fresh air variables shall be the follows:
 $\omega [\text{rpm}] \rightarrow \dot{V}_{so} [\text{m}^3/\text{h}] \rightarrow T_{si} [^\circ\text{C}] \rightarrow \phi_{ei} [\%]$.
- The duration of measurements was at least 300 seconds at intervals of 2 seconds.
- The sequence of measurements was determined so that the difference between desired temperature and humidity values was minimal. This helped reaching the stationary state of operation faster.

Calculation of the energy wheel effectiveness by using the experimental data

The effectiveness eqs. (1)-(3) proposed by ASHRAE Standard 84 [22] that is used in this work is defined in the equations below as the effectiveness is given as sensible effectiveness (heat transfer process), latent effectiveness (moisture transfer process), and total effectiveness (total energy transfer including heat and moisture transfer).

The methodology is based on air temperature and air humidity measurements on the inlet and outlet parts of the energy wheel under steady-state conditions:

$$\varepsilon_s = \frac{\dot{m}_{si}(T_{si} - T_{so})}{\text{Min } \dot{m}_{si}, \dot{m}_{ei}(T_{si} - T_{ei})} \quad (1)$$

$$\varepsilon_L = \frac{\dot{m}_{si}(X_{si} - X_{so})}{\text{Min } \dot{m}_{si}, \dot{m}_{ei}(X_{si} - X_{ei})} \quad (2)$$

$$\varepsilon_T = \frac{\dot{m}_{si}(h_{si} - h_{so})}{\text{Min } \dot{m}_{si}, \dot{m}_{ei}(h_{si} - h_{ei})} \quad (3)$$

The supply and exhaust mass flow rate are calculated from:

$$\dot{m} = \rho_a \dot{V} \quad (4)$$

The sensible effectiveness can be calculated directly as the dry bulb temperature can be substituted in the equation with no need to convert. While the latent and total effectivenesses were calculated after obtaining the values for absolute humidity and specific enthalpy from:

$$x = 0.622 \frac{p_w}{p_a - p_w} \quad (5)$$

$$h = C_{p,a} T + x(C_{p,y} T + h_{fg}) \quad (6)$$

Results and discussion

Using the measured data, the calculated sensible, latent and total effectiveness values of the tested energy wheel at different operation and ambient parameters and correlation between the wheel and different parameters will be presented in this section.

All results were obtained under $T_{ei} = 22$ °C and $\phi_{ei} = 35\%$ constant exhaust air parameters and in the range of supply air temperature, T_{si} , between -15 to 0 °C and at supply relative humidity, RH_{si} , 100% . In summer condition, the results obtained for $T_{ei} = 24$ °C and $\phi_{ei} = 45\%$ constant exhaust air parameters and in the range of supply air temperature 5 – 40 °C and supply air relative humidity varied depending on the experimental process.

Sensible effectiveness vs. dry-bulb temperature

Figure 2 presents the sensible effectiveness vs. dry bulb temperature under different volume flow rates at the maximum wheel speed, $\omega = 20$ rpm. It seems, from trending data, the maximum sensible effectiveness occurs at the lowest air volume flow rate. However, the trend for every volume flow rate shows almost the same values at different temperatures.

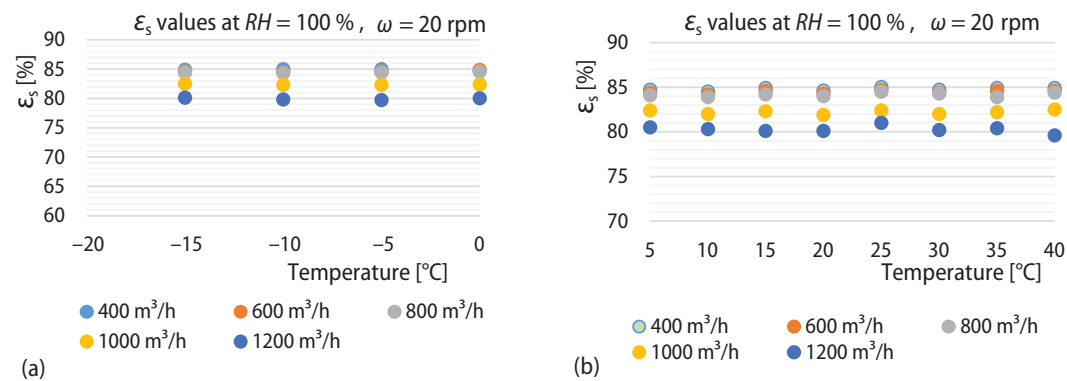


Figure 2. Sensible effectiveness [%] vs. dry bulb temperature [°C] at different air volume flow rate and at $\omega = 20$ rpm; (a) winter condition, (b) summer condition (for color image see journal web site)

Latent effectiveness vs. wheel speed

Latent effectiveness was more sensitive for wheel rotation speed step changing under the same air volume flow rate and different supply inlet temperature conditions, fig. 3. It can

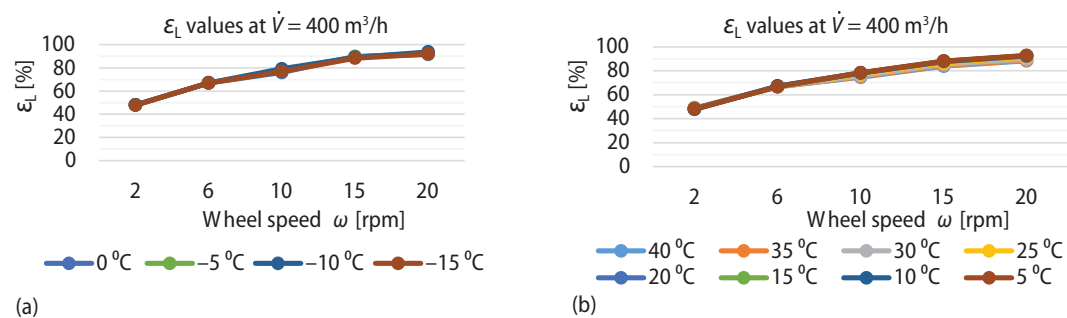


Figure 3. Latent effectiveness [%] vs. wheel speed [rpm] at different dry bulb temperature [°C] and at $\dot{V} = 400$ m³/h; (a) winter condition, (b) summer condition (for color image see journal web site)

be realized, from trending data, the maximum Latent effectiveness occurs at the highest wheel speed. However, the temperatures show almost the same trend at different wheel speeds.

Total effectiveness vs. wheel speed

Figure 4 below presents the total effectiveness vs. wheel speed for different dry bulb temperature at $\dot{V} = 400 \text{ m}^3/\text{s}$, it can be realized, from trending data, the maximum total effectiveness occurs at the highest wheel speed. However, the temperatures show almost the same trend at different wheel speeds.

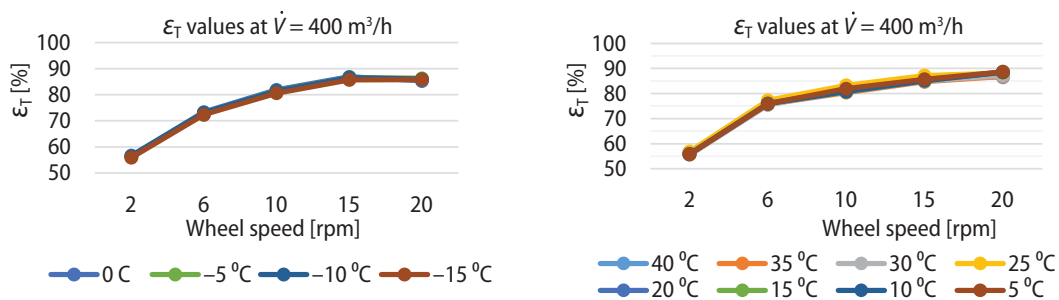


Figure 4. Total effectiveness [%] vs. wheel speed [rpm] at different dry bulb temperature [°C] and at $\dot{V} = 400 \text{ m}^3/\text{h}$; (a) winter condition, (b) summer condition (for color image see journal web site)

Maximum effectiveness vs. dry-bulb temperature

Figure 5 shows that all the effectivenesses values in the function of dry bulb temperature levels at lowest volume flow rate, $\dot{V} = 400 \text{ m}^3/\text{s}$, and maximum wheel speed, $\omega = 20 \text{ rpm}$. It can be obtained, from trending data that the maximum effectiveness is the latent effectiveness overall at the same operating parameters which reaches almost 94 %.

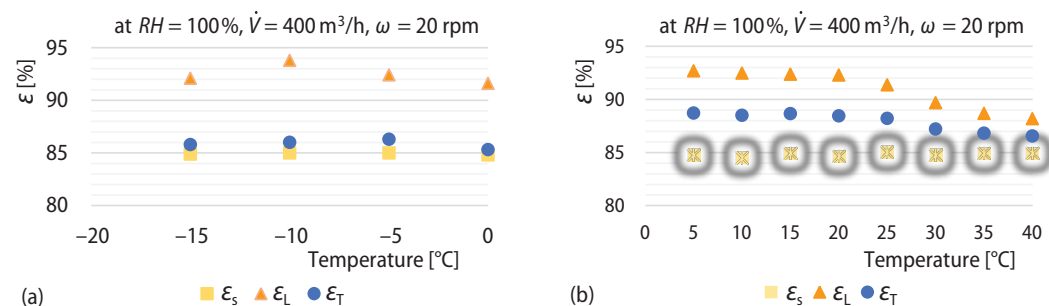


Figure 5. Maximum effectiveness [%] vs. dry bulb temperature [°C] for effectiveness at $\omega = 20 \text{ rpm}$ and at $\dot{V} = 400 \text{ m}^3/\text{h}$; (a) winter condition, (b) summer condition (for color image see journal web site)

Latent and total effectiveness vs. relative humidity

Figure 6 below presents the latent and total effectiveness in the function of relative humidity for different dry bulb temperature [°C] at $\dot{V} = 400 \text{ m}^3/\text{s}$ air volume flow rate. It can be realized, from trending data that the maximum latent and total effectiveness occurs at the lowest temperature. However, the effectiveness increased when the relative humidity decreased for different temperatures.

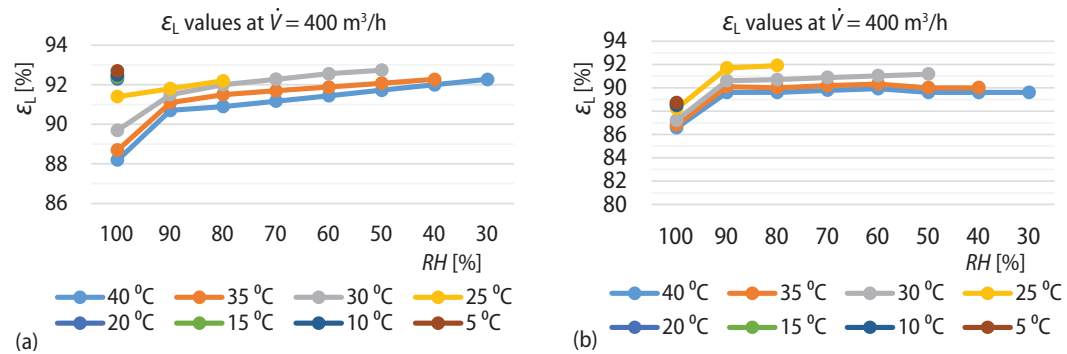


Figure 6. Latent (a) and total (b) effectiveness [%] vs. relative humidity [%] at different dry bulb temperature [°C] and at $\dot{V} = 400 \text{ m}^3/\text{h}$ (for color image see journal web site)

Uncertainty in calculating the effectiveness

Kline *et al.* [23] have presented the method used for estimating uncertainty in experimental results as shown in the eq. (7). The method is constructive on precise specifications of uncertainties in the many primary experimental measurements [24]. It is more clear to define the experimental uncertainties, eq. (7) rather than to experimental errors in the experiments. The analysis combines all the errors in the results<

$$\omega_R = \pm \sqrt{\left(\frac{\partial R}{\partial x_1} \omega_{x_1} \right)^2 + \left(\frac{\partial R}{\partial x_2} \omega_{x_2} \right)^2 + \dots + \left(\frac{\partial R}{\partial x_n} \omega_{x_n} \right)^2} \quad (7)$$

The temperature and relative humidity sensors were located in the mid-section in the test facility before and after the energy wheel. The calibration result for the humidity and temperature metering instrument and the hot-wire anemometer can be shown in tab. 5.

Table 5. Calibration result of the multifunction instrument

Nominal value	Normal value	Measured value	Deviation	Uncertainty
40% RH	39.9% RH	40.5% RH	0.6% RH	0.5 % RH
0 °C	0.09 °C	0.3 °C	0.21 °C	0.08 °C
1 m/s	0.98 m/s	1.00 m/s	0.02 m/s	0.05 m/s

As sample the description under below shows how the uncertainty in the effectiveness were calculated during our research.

Data observed and measured:

- Volumetric flow rate = $400 \text{ m}^3/\text{h}$
- Temperature of the supply inlet = -15 °C
- Relative humidity of the supply inlet = 100%
- Temperature of the exhaust inlet = 22 °C
- Relative humidity of the exhaust inlet = 35%

The eqs. (8)-(10) show the calculations of uncertainty in sensible, latent and total effectivenesses:

$$\omega_{\epsilon_s} = \pm \sqrt{\left(\frac{\partial \epsilon_s}{\partial \dot{m}_{si}} \omega_{\dot{m}_{si}} \right)^2 + \left(\frac{\partial \epsilon_s}{\partial T_{si}} \omega_{T_{si}} \right)^2 + \left(\frac{\partial \epsilon_s}{\partial T_{so}} \omega_{T_{so}} \right)^2 + \left(\frac{\partial \epsilon_s}{\partial T_{ei}} \omega_{T_{ei}} \right)^2} = \pm 3.72\% \quad (8)$$

$$\omega_{\varepsilon_L} = \pm \sqrt{\left(\frac{\partial \varepsilon_L}{\partial \dot{m}_{si}} \omega_{\dot{m}_{si}}\right)^2 + \left(\frac{\partial \varepsilon_L}{\partial x_{si}} \omega_{x_{si}}\right)^2 + \left(\frac{\partial \varepsilon_L}{\partial x_{so}} \omega_{x_{so}}\right)^2 + \left(\frac{\partial \varepsilon_L}{\partial x_{ei}} \omega_{x_{ei}}\right)^2} = \pm 5.93\% \quad (9)$$

$$\omega_{\varepsilon_T} = \pm \sqrt{\left(\frac{\partial \varepsilon_T}{\partial \dot{m}_{si}} \omega_{\dot{m}_{si}}\right)^2 + \left(\frac{\partial \varepsilon_T}{\partial h_{si}} \omega_{h_{si}}\right)^2 + \left(\frac{\partial \varepsilon_T}{\partial h_{so}} \omega_{h_{so}}\right)^2 + \left(\frac{\partial \varepsilon_T}{\partial h_{ei}} \omega_{h_{ei}}\right)^2} = \pm 6.77\% \quad (10)$$

Figure 7 shows the uncertainties for all the effectiveness values in the function of dry bulb ambient temperature for summer and winter condition at lowest volume flow rate, $\dot{V} = 400 \text{ m}^3/\text{s}$ and maximum wheel rotation speed, $\omega = 20 \text{ rpm}$.

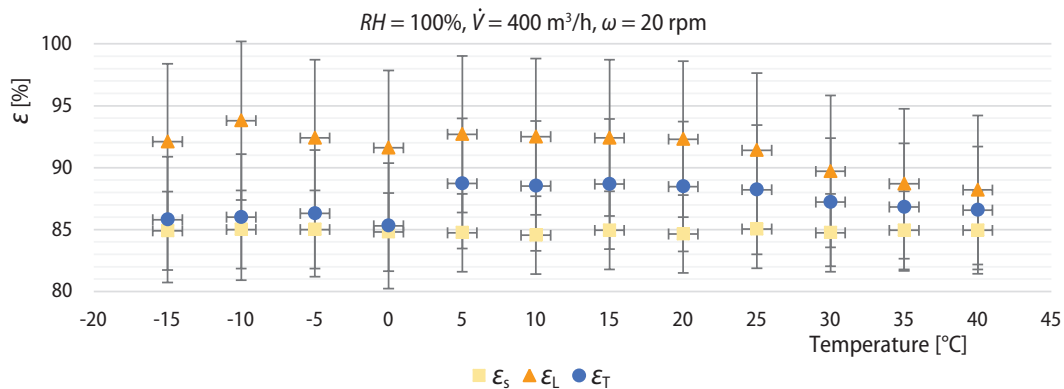


Figure 7. Uncertainty in effectiveness [%] vs. dry bulb temperature [°C] for effectiveness at $\omega = 20 \text{ rpm}$ and at $\dot{V} = 400 \text{ m}^3/\text{h}$ (for color image see journal web site)

Conclusions

In this work, experimental tests were conducted to determine sorption energy wheel performance. The performance of the sorption wheel was evaluated under extreme wide range ambient air condition parameters. The major findings obtained from research work are summarized as follows.

- The sensible effectiveness obtained from the experiments showed an increasing trend by decreasing the air volume flow rate under winter and also summer ambient air conditions. However, the results show almost the same sensible effectiveness values under different dry bulb air temperatures and same wheel rotation speeds.
- It could be obtained that the values of the sensible effectiveness start to reduce when wheel speed reaches a value of 10 rpm and lower.
- The latent and total effectivenesses showed an increasing trend by decreasing the air volume flow rate and increasing the wheel rotation speed.
- The latent and total effectiveness values have a maximum value under wheel speed 20 rpm, and decrease constantly as a function of rpm.
- It can be obtained from all the test data that the peak value of the latent effectiveness reached almost 94%.
- The maximum latent and total effectiveness values were found at the lowest ambient air dry bulb temperatures.
- The latent and total effectiveness values increased by decreasing the relative humidity of the ambient air under different temperature levels.

Acknowledgment

This research project was financially supported by the National Research, Development and Innovation Office from NRD Fund. Grant number: NKFIH PD_18 127907, the Janos Bolyai Research Scholarship of the Hungarian Academy of Sciences, and the UNKP-18-4 New National Excellence Program of the Ministry of Human Capacities, Budapest, Hungary.

Nomenclature

C_p – specific heat capacity, [$\text{kJkg}^{-1}\text{K}^{-1}$]
 h – enthalpy, [kJkg^{-1}]
 \dot{m} – mass flow rate, [kgs^{-1}]
 p – partial pressure, [Pa]
 R – function of a desired result, [–]
 T – dry bulb temperature, [$^{\circ}\text{C}$]
 \dot{V} – volume flow rate, [m^3s^{-1}]
 x – absolute humidity, [kgkg^{-1}]

Greek symbols

ρ – density, [kgm^{-3}]
 ε – effectiveness of sorption wheel, [–]
 ω – wheel rotation speed [rpm]
 ω_R – uncertainty for R function, [–]

ω_x – uncertainty for the independent, [–]
 φ – relative humidity, [%]

Subscripts

a – moist air
 ei – exhaust inlet
 eo – exhaust outlet
 L – latent
 uk – supply inlet
 uq – supply outlet
 s – sensible
 T – total
 w – water vapor

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