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#### Review 2

# Fermentative hydrogen production in anaerobic membrane bioreactors:

## 6 4 7 A review 5

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ABSTRACT

ventional CSTR counterparts.

HIGHLIGHTS

15 • Anaerobic, integrated membrane bioreactors (AnMBRs) are reviewed.

16 Specific AnMBR applications for biohydrogen production are discussed.

• Hydrogen generation possibilities and potentials in AnMBRs are critically evaluated. 17

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# 1. Introduction

Hydrogen represents one of the highly attractive directions in 48 alternative energy research (Winter, 2009). It is an environmen-49 50 tally gentle compound which can be formed by several biological ways including both the light-dependent and dark fermentative 51 processes (Show et al., 2012). Nowadays, considering practicality 52 aspects, the latter class seems more feasible and therefore not only 53 receives high scientific attention in laboratories but also there is a 54 55 remarkable, ongoing progress towards scaling-up. As a result, a 56 couple of pilot plants have recently been established (La Licata 57 et al., 2011; Lin et al., 2011) and demonstration as well as full-scale 58 facilities may be expected (Guo et al., 2010). Although fermentative hydrogen production is undoubtedly promising and it is devel-59 60 oping step by step to a level of real field applications, scientists need to spend additional efforts to enhance the overall process effi-61 62 ciency, preferentially by using waste materials (Sinha and Pandey, 2011). In particular, from the upstream point of view, further 63 advancements are essential to attain better generation rates and 64

yields so that hydrogen can be made more competitive with other energy carriers e.g. in economical terms (Hallenbeck and Ghosh, 2009). Nevertheless, it has been shown that the fate of biohydrogen is also dependent on the successfulness of the downstream technology which may contribute to the intensification of the production side (Bakonyi et al., 2013).

Reactor design considerations are crucial aspects of dark fermentative hydrogen production. During the

last decades, many types of reactors have been developed and used in order to drive biohydrogen tech-

nology towards practicality and economical-feasibility. In general, the ultimate aim is to improve the key

features of the process, namely the H<sub>2</sub> yields and generation rates. Among the various configurations, the

traditional, completely stirred tank reactors (CSTRs) are still the most routinely employed ones. However,

due to their limitations, there is a progress to develop more reliable alternatives. One of the research

directions points to systems combining membranes, which are called as anaerobic membrane bioreactors

(AnMBR). The aim of this paper is to summarize and highlight the recent biohydrogen related work done

on AnMBRs and moreover to evaluate their performances and potentials in comparison with their con-

Hence, various biological and engineering approaches have been suggested with the aims mentioned, such as the construction of more sufficient and robust hydrogen producer microorganisms (metabolic- and genetic engineering), fermentation optimization and bioreactor design (Guo et al., 2010). All of these approaches possess high importance because strains require proper surroundings (e.g. pH, temperature, H<sub>2</sub> partial pressure, mass transfer, etc.) to express their advantageous properties (Wang and Wan, 2009). Moreover, since bioreactors are the places of the microbiological hydrogen conversion, their quality features such as type and configuration significantly affect the applications reliability. In the last decade, as a response to the demand for biosystems with upgraded hydrogen generation performance, several researchers have started to deal with the novel and innovative way of combining traditional hydrogen fermenters with membrane technology. Recently, our group comprehensively assessed the integration

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87 possibilities of membranes and bioreactors for biohydrogen recov-88 ery and enrichment in gas separation membrane bioreactors (Bak-89 onyi et al., 2013) or in other words, in hydrogen extractive 90 membrane bioreactors (Ramírez-Morales et al., 2013). This is one 91 particular way to establish membrane-based systems for fermentative hydrogen technology. Another one is the design of anaerobic 92 93 bioreactors employing membranes in the liquid phase, which are 94 in the scope of the present paper. Although a couple of review papers have recently been published on anaerobic membranes biore-95 96 actors (AnMBR) (Lin et al., 2013; Ozgun et al., 2013; Singhania et al., 97 2012; Smith et al., 2012) and their potential for hydrogen produc-98 tion was enlightened (Gallucci et al., 2013; Jung et al., 2011), H<sub>2</sub> production in systems combining liquid filtration membranes has 99 not specifically been addressed and evaluated so far. 100

101 Therefore, this work attempts to overview the progress on the 102 anaerobic membrane bioreactors used in the fermentative hydro-103 gen technology. Firstly, the main features of conventional, anaero-104 bic membrane bioreactors are presented. Thereafter, several main 105 process considerations (retention time, nutrient loading, mem-106 brane related issues) affecting the performance of anaerobic hydro-107 gen producing membrane bioreactors (AnHPMBR) are discussed. 108 Finally, the feasibility of AnMBRs for biological hydrogen generation in comparison to the traditional CSTRs will be evaluated. 109

## 110 2. General features of AnMBR systems

AnMBRs have been used for a long time in different fields, mostly in waste water treatment for process intensification purposes even at full-scale plants (Judd, 2008).

114 Integrated systems assisted by membranes – being either 115 aerobic or anaerobic and regardless the purpose of use – can be 116 distinguished as external loop (Fig. 1A) and submerged (Fig. 1B) 117 bioreactors (Yang et al., 2006). In the former case, as indicated in 118 Fig. 1A, the liquid filtration membrane module is linked to the 119 reactor from outside and handles the circulating fermentation broth. In the latter solution, as demonstrated in Fig. 1B, the membrane module is sunk in the liquid phase of the reactor vessel or sometimes immersed in a separate tank.

Both types of bioreactors have their own advantages and disadvantages. Basically, the external loop arrangement is recognized with a higher operation energy demand but cleaning and replacement of the membrane is easier to perform. On the other hand, submerged membrane bioreactors are less energy intense but require larger membrane surface area to ensure sufficiently high permeate fluxes in comparison to their external loop counterparts (Lin et al., 2013). As foreshadowed in Figs. 1B and 2, AnMBRs can be operated in bubble coarse mode when headspace gases are recycled to the bottom of the reactor through diffusers or spargers. On one hand, it can help mixing and gas bubbles contacting the membrane surface may contribute to reduce the developing cake layer. On the other hand, continuous gas flushing can improve the liquid to gaseous phase mass transfer rate so that dissolved gases are more efficiently removed. Theoretically, it is desirable in the case of dark fermentative hydrogen production since the catalytic activity of hydrogenase enzymes can be sensitive to increasing H<sub>2</sub> concentrations in the aqueous phase (Bakonyi et al., 2013; Hallenbeck, 2009; Nath and Das, 2004; Ramírez-Morales et al., 2013).

Taking into account the possible reactor configurations, membranes are most commonly joined to completely stirred tanks. However, there are some alternative solutions such as certain kinds of upflow- and granular sludge bioreactors (Ozgun et al., 2013). From the viewpoint of the membrane, it can be noticed that membranes made of several commercial polymers e.g. PE, PP, PVDF, etc. are preferentially applied due to process economical reasons. These materials are often built into flat sheet and tubular modules. Furthermore, the hollow fiber configuration is also favorable because of its high packing density (Santos and Judd, 2010).

In general, based on the experiences with anaerobic membrane bioreactors their implementation could appear to be prosperous but it is important to note their limits and drawbacks. It is a common observation that in integrated systems – combining





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Fig. 2. Cake formation during cross-flow filtration in anaerobic membrane bioreactors.

(1)

liquid/solid separation membranes and bioreactors - fouling is a 156 potential threat (Gallucci et al., 2013; Lin et al., 2013). If occurs, 157 158 it is accompanied by an increased membrane resistance and hence it lowers the most important trait, the flux of the membrane 159 (Fig. 2) and may cause operational failures (e.g. shortened mem-160 brane lifetime). Thus, fouling inherently affects the process econ-161 omy and should be restricted as much as possible. The overall 162 resistance of the membrane  $(R_o)$  – expressed by Eq. (1) – is a prod-163 uct of various terms such as the inherent membrane resistance 164  $(R_{\rm m})$ , the resistance of the cake layer  $(R_{\rm g})$ , the resistance caused 165 by pore plugging  $(R_p)$  and the resistance associated with biological 166 167 activity referring to biofouling  $(R_b)$  e.g. biofilm formation.

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$$70 \qquad R_o = R_m + R_c + R_p + R_b$$

171 The sustainability of membrane performance is dependent on a 172 few factors related to the operational circumstances (e.g. shear rate 173 on the membrane surface, operational flux, separation tempera-174 ture, hydraulic- and solid retention times, etc.), membrane characteristics (e.g. pore diameter – usually  $0.2-1 \mu m$ , hydrophobicity) 175 and the qualities of the media to be filtrated (e.g. composition, 176 microbial community structure, solid particulate size) (Calderón 177 178 et al., 2011; Gao et al., 2010, 2011; Liao et al., 2006; Lin et al., 2010; Meng et al., 2009; Ozgun et al., 2013; Singhania et al., 179 180 2012; Smith et al., 2012; Szentgyörgyi and Bélafi-Bakó, 2010; 181 Wijekoon et al., 2011).

In case the membrane usability reaches an insufficient level due 182 183 to the reasons mentioned above, users can turn to various on phys-184 ical, chemical or enzymatic techniques in order to suppress fouling. 185 The physical ones comprise backwashing, membrane relaxing (Le-Clech et al., 2006) and recently vibration through exposure to 186 ultrasonic irradiation receives noticeable research interest (Sui 187 et al., 2008; Wen et al., 2008). However, these approaches have 188 189 limited effectiveness and in many cases the troubleshooting of fouling demands more drastic methods such as adding chemicals 190 191 which encompass bases e.g. NaClO, NaOH and acids e.g. citric-, hydrochloric-, nitric or other agents such as EDTA or ozone (Lin 192 et al., 2013; Sun et al., 2011b). Although these processes are 193 194 mature and routinely used to recover membrane performance, 195 they might damage the membrane itself (Drews, 2010) and hence 196 alternative biological direction, namely the enzymatic treatment has been proposed by a couple of investigators (Allie et al., 2003; 197 198 Maartens et al., 2002; te Poele and van der Graaf, 2005).

Furthermore, the external addition of so-called flux enhancers (e.g. poly-aluminum chloride, powdered activated carbon) is also a realistic option to hinder permeability decrease (Aun Ng et al.,2012013; Ozgun et al., 2013).202

## 3. Biohydrogen production in anaerobic membrane bioreactors 203

## 3.1. The effect of solid- and hydraulic retention times in AnHPMBRs 204

Hydrogen bioproduction by continuous cultures is frequently carried out in well-mixed vessels in which proliferation of microorganisms is determined by the dilution rate applied, presenting a potential risk for biomass washout (Li and Fang, 2007; Show et al., 2008). Therefore, decoupling hydraulic- (HRT) and solid/biomass retention times (SRT) in anaerobic, hydrogen producing bioreactors (Table 1) possesses several benefits.

Preserving cells in continuous bioreactors can be accomplished in several alternative ways such as the immobilization and recycling of the suspended cells. However, the former may suffer from mass transfer limitations due to the slow diffusion rate of substrates through biofilms or carrier matrices (e.g. alginate beads) that represent an apparent limitation during the process. Nevertheless, retraining cells in a suspended form may help to avoid diffusion limitations. Nowadays, such cell-retention devices ensuring a sufficiently long SRT are attractively designed by using membranes and refer to *anaerobic hydrogen producing membrane bioreactors*.

Previously, tt has been well demonstrated that maintaining longer SRT and shorter HRT might improve the bioH<sub>2</sub> generation efficiency (Hafez et al., 2009). This is because in such systems a more substantial population of active H<sub>2</sub> producer strains can be provided and it expectedly results in a higher biogas turnout and substrate conversion (Jung et al., 2011;Melin et al., 2006) especially when poorly soluble and slowly biodegradable raw materials are the targets of the fermentation (Meabe et al., 2013).

Although it seems that independent solid- and hydraulic retention times are key process variables for a more promising hydrogen production their values should carefully be chosen since it is possible that an immoderate solid retention time decreases the hydrogen formation capacity. Moreover, in general, the levels of HRT and SRT were demonstrated to have an adverse effect on hydrogen yield and volumetric productivity, meaning that peak values may occur under distinct operational (retention time) conditions (Lee et al., 2007; 2010; Kim et al., 2011). Besides, the impacts of SRT could be correlated with the formation of extracellular polymeric substances (EPS), as well. The release of EPS is usually more intense at elevated SRTs and the accumulation of such metabolic side-

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#### Table 1

Performances of anaerobic membrane bioreactors employed for hydrogen fermentation.

Inoculum	Substrate	Retention time		H <sub>2</sub> generation performance (highest values)		Reference
		Hydraulic	Solid/Biomass	Yield	Productivity	
Heat-treated soil inocula	Glucose	3.3-5	3.3–48 h	N.S.	9.2 L H <sub>2</sub> /L-d	Oh et al. (2004)
Acid-treated, acclimated sludge	3 Hexoses	1–4 h	N.S.	39 L H <sub>2</sub> /mol glucose	66 L H <sub>2</sub> /L-d*	Lee et al. (2007)
Heat-treated sludge	Glucose	9 h	450 d	N.S.	2.5 L H <sub>2</sub> /L-d	Lee et al. (2008)
Screened anaerobic digester sludge	Glucose	8 h	24 h	40.2 L H <sub>2</sub> /mol glucose	4.5 L H <sub>2</sub> /L-d	Shen et al. (2009)
Heat-treated sludge	Glucose	9 h	12.5 h	35.4 L H <sub>2</sub> /mol glucose	5.9 L H <sub>2</sub> /L-d	Lee et al. (2009a)
Heat-treated, acclimated sludge	Glucose	N.S.	90 d	19.5 L H <sub>2</sub> /mol glucose	2.5 L H <sub>2</sub> /L-d	Lee et al. (2009b)
Heat-treated, acclimated sludge	Glucose	9 h	2-90 d	27 L H <sub>2</sub> /mol glucose	5.8 L H <sub>2</sub> /L-d	Lee et al. (2010)
Acclimated sludge	Glucose	8 h	24 h	N.S.	4.4 L H <sub>2</sub> /L-d	Shen et al. (2010)
Heat-treated sludge	TPW	2–8 h	N.S.	42.4 L H <sub>2</sub> /mol hexose**	19.8 L H <sub>2</sub> /L-d	Kim et al. (2011)

N.S.: not specified; TPW: Tofu processing waste; \*: on fructose; \*\*: hexose added.

products within the reactor may be accountable for the inhibition of  $H_2$  evolution (Lee et al., 2010).

244 Nevertheless, the literature is not consistent regarding the opti-245 mal set of SRT. For example, one study found the 90 days long SRT 246 already unfavorable (Lee et al., 2010), meanwhile another 247 AnHPMBR with extreme solid rejection time as long as 450 days was possible to run without observing any undesired performance 248 249 loss in terms of hydrogen generation (Lee et al., 2008). These re-250 sults imply a need for the system- or case-specific determination 251 of the most proper SRT similarly to the case of HRT which is another indicator that allows elucidating the behavior of an 252 253 AnHPMBR. For instance, varying the HRT can change the nutrients loading rate and thus it likely alters the utilization efficiency of 254 255 substrates fed and concomitantly the achievable bioreactor perfor-256 mance, as well (Lee et al., 2007; Oh et al., 2004).

257 Furthermore, alterations in SRT may lead to a remarkable shift 258 in the microbial diversity which in turn is able to directly and com-259 pletely divert the reactor behavior to a new state being perhaps 260 accompanied by a different biohydrogen production pattern (Oh 261 et al., 2004). This can be attributed to the fact that extended biomass residence time can not only accelerate the proliferation of 262 263 H<sub>2</sub> evolving bacteria but also that of the competitive and hydro-264 gen-consuming microbes (e.g. methanogenes, homoacetogenes, 265 etc.), or in other words, the population composition can change 266 due to the appearance of new, dominant organisms. Nevertheless, 267 to be straightforward, none of the relevant works in the literature 268 reported on appearing methanogenic activity, not even when high SRT values were maintained. Therefore, addressing the microbial 269 270 community aging along with SRT deviation can be an interesting 271 object of future investigations.

It is to conclude that though membrane bioreactors are quite frequently employed e.g. for the purpose of biological wastewater treatment as stated above, their applicability in the field of biohydrogen has not reached such dimensions up to now. Hence, these applications should grow to a wider recognition.

#### 277 3.2. Effect of nutrient loading in AnHPMBRs

The availability of nutrients comprising carbon sources and other substances such as mineral salts is a crucial issue not only in standard free cell- but also in membrane-coupled bioreactors. The first group usually takes the role of substrates that are bioconverted into molecular hydrogen gas.

The hydrogen formation biosystems in AnMBRs design are constructed with the aim of improving the generation efficiency as compared to CSTRs both in terms of  $H_2$  yields and production rates under versatile circumstances e.g. operated with various substrate loading rates. However, the relevant studies on this subject did not provide definitive answers so far whether the deployment of AnHPMBRs could lead to prominent hydrogen formation capacities when testing with different organic loading rates (OLR). In fact, some authors communicated declined H<sub>2</sub> yields and mostly lower H<sub>2</sub> evolution rates in AnMBR mode (Shen et al., 2009). In contrast, other report justified the excellence of AnHPMBR operation over a wide range of organic matter loadings although it showed certain substrate specific dependency (Lee et al., 2007). Additionally, it has been found that a gradually increased OLR (from 4 to 22 g COD/L-d) could aid the H<sub>2</sub> production but the excessively high levels (30 g COD/L-d) caused a noticeable (20%) depression in the gas generation performance (Shen et al., 2010).

Moreover, the degradation efficiency of substrate introduced to the bioreactor was shown to be considerably influenced by the SRT applied, indicating that a sufficiently prolonged solid retention may be a key factor for a better microbiological uptake and organic matter transformation (Lee et al., 2010). Furthermore, Shen et al. (2010) investigated the impact of OLR on the features (concentration, mean diameter) of colloidal organic matter (polysaccharides and proteins) in AnHPMBRs, however, no clear correlations were identified between the factors.

As indicated at the beginning of this section, minor elements present in the broth can strongly affect the successfulness of the hydrogen fermentation in AnMBRs, depending on their concentrations. Accordingly, the iron level of the media is designated as an important variable since it can either improve or suppress the process. It is explained by the fact that most H<sub>2</sub>-evolver enzymes are characterized with Fe-content in their active core/site. Thereby, sustainable H<sub>2</sub> production in AnHPMBRs needs proper iron supplementation (Lee et al., 2009a) so that Fe can be utilized as a building element of hydrogenases. However, Fe should not be supplied above a certain tolerable concentration otherwise strains get overloaded and subsequently poisoned that easily leads to reduced hydrogen formation efficiency.

Though several conclusions could be drawn concerning the impact of nutrient loading in AnHPMBRs, further research seems essential with various, currently untested and preferentially complex materials in order to increase the knowledge about the substrate quality- and quantity-dependent behavior of fermentative biohydrogen systems employing membranes.

#### 3.3. The issue of membrane fouling in AnHPMBRs

The microbiological processes themselves can have a notable329impact on the overall performance of membranes applied in330AnHPMBRs (Table 2) which is a consequence of the metabolic331product release of the strains present.332

In this regard, the formation of EPS such as proteins, polysaccharides, etc. and biopolymer clusters can increase fermentation liquor viscosity and promote biofilm formation on the surface of the 335

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Fable 2
Specific characteristics of anaerobic membrane bioreactors used for fermentative hydrogen production

Type of	Membrane	Reference				
AnMBR	Configuration Surface area (m <sup>2</sup> )/Pore size (µm)		Material	Type of membrane	Supplier	
External-loop	Tubular	0.0055/0.2-0.8	Ceramic	Membralox®	US Filter Co.	Oh et al. (2004)
External-loop	Hollow-fiber	0.1/0.2	PP	MicroDyn MD020CP2 N	Mycrodyn-Nadir GmbH	Lee et al. (2007)
Submerged	Plate-flame	0.1/0.45	PE	Microfiltration	Kubota Co.	Lee et al.(2008)
Submerged	Hollow-fiber	0.047/0.04	PVDF	ZeeWeed <sup>®</sup> ultrafiltration	GE Water and Process	Shen et al. (2009,
				module	Technologies	2010)
Submerged	Plate-flame	0.1/0.45	PE	Microfiltration	Kubota Co.	Lee et al. (2009a)
Submerged	Plate-flame	0.1/0.45	PE	Microfiltration	Kubota Co.	Lee et al. (2009b)
Submerged	Plate-flame	0.1/0.45	PE	Microfiltration	Kubota Co.	Lee et al. (2010)
External-loop	Hollow-fiber	0.025/N.S.	N.S.	Microfiltration	N.S.	Kim et al. (2011)

N.S.: not specified.

membrane. Consequently, it may lead to (bio)fouling with a
concurrent increase in membrane transport resistance and thereby
an unsteady operation (Choi et al., 2005; Choo and Lee; 1996; Ramesh et al., 2006; Sun et al., 2008, 2011a; Wang and Li, 2008).

On the other hand, EPS could also express a particularly advantageous effect since they play a main role in the granulation of the
microorganisms (Hung et al., 2011), which may govern the hydrogen producing biosystem towards better stability and a more viable performance.

345 As specified in Section 3.1., the intensity of EPS formation is likely a function of the SRT applied. Therefore, the extent of captur-346 347 ing suspended solids inside the bioreactor, or in other words, the 348 accumulated concentration of certain substances (covering cell-349 mass, as well) is denoted as a potential factor influencing the mem-350 brane's usability. It is because (colloidal) compounds as well as 351 microorganisms can be deposited and adhered on the membrane 352 surface that potentially cuts down the achievable permeate flux in AnHPMBRs (Shen et al., 2010). Upon the sedimentation of living 353 cells onto the membrane interface, biofilm may start to develop 354 and increase the risk of biofouling. (Habimana et al., 2014). Simi-355 larly to microbes, EPS are typically neither allowed to pass through 356 357 the liquid filtration membrane unit and may be bound to the phase 358 barrier surface, inducing severe biofouling. Moreover, it has been 359 elucidated that EPS – because of their pendant functional groups 360 - can likely form complexes with metal cations and/or other ligands present in the fermentation broth. As it has turned out, this 361 362 phenomenon may not only influence micronutrient availability but also depress permeate flux in membrane-based biohydrogen pro-363 duction reactors (Lee et al., 2008). Apart from the concentration 364 365 of EPS, suspended organic matter and bacterial cell mass, mem-366 brane permeate flux in AnHPMBRs reflects a dependency on parameters such as transmembrane pressure, cross-flow velocity 367 368 and membrane pore diameter (Oh et al., 2004).

Consequently, membrane durability in AnMBRs is apparently determined by two main groups of variables associated with (1) biological phenomena e.g. EPS release, <u>cell-surface</u> interactions and (2) membrane operation.

However, membrane fouling may take place regardless the membrane operational conditions in AnHPMBRs and occasional regeneration e.g. regular backwashing should be applied to control the phenomena (Oh et al., 2004).

Although anaerobic hydrogen producing membrane bioreactors can suffer from membrane fouling (Lee et al., 2010) e.g. as a result of EPS accumulation, cake formation, high solid (colloidal particle) content, biological growth (biofilm development on the membrane surface) it does not inevitably happen according to the experiences. A couple of literature reports state that it was possible to run the  $H_2$  generation bioreactor for a long time without any membrane-related operational failures (Kim et al., 2011; Lee et al., 2007). This is of significance because each membrane is contributed with cost- and lifetime factors which substantially determine the (larger-scale) feasibility of AnMBRs for biohydrogen generation.

Nevertheless, the phenomenon of membrane fouling in AnHPMBRs deserves a more particular evaluation. Basically, in continuous bioreactors, the SRT/HRT ratio defines a so-called concentration factor for the solid compounds in the broth. As can be seen in Table 1, the relevant studies employed quite distinct SRT/ HRT ranging from low and moderate (Oh et al., 2004; Lee et al., 2009a, 2010; Shen et al., 2009) to extremely high values (Lee et al., 2008, 2010). Basically, increasing the SRT/HRT factor yields higher metabolite and suspended solid concentrations under steady-state bioreactor conditions, moreover, it causes the reduction of the permeate fluxes. It is attributable to the fact that during membrane (micro)filtration the streams containing more substances are more difficult to be filtrated (Lee et al., 2008; Oh et al., 2004) since the composition of the media significantly determines the filtration performance.

As a summary, separate HRT and SRT values in AnHPMBRs should be set to obtain a higher biomass density, however it may lead to undesired alterations in membrane effluent fluxes. In case of intolerably decreased liquid permeation, intermittent backwash and relaxing of the membrane may help to recover the performance though these techniques were found to be effective only for relatively short-terms (Lee et al., 2008; Oh et al., 2004). Another way to reclaim decent filtration rate is increasing the driving force (transmembrane pressure difference) of the process. Although enhancing the pressure ratio between the primary and secondary sides of the membrane module sounds quite logical to sustain the intended permeate fluxes, such strategy may lead to undesired consequences in membrane usability. This can be made clear by taking into account the contributions of various factors to the overall membrane resistance (see Eq. (1)). At the beginning of the AnMBR operation when the concentration of solids in the fermentation liquor is relatively lower, suspended solids and colloids start to accumulate on the membrane surface and the developing cakeand gel layer resistances are dominant (Lee et al., 2008). Depending on their thickness, these depositions obstruct the movement of the flowing liquid across the membrane and therefore flux may gradually decline (Fig. 2). At that point if a higher transmembrane pressure gradient is adjusted in order to fix the permeation properties, substances from the surface of the membrane penetrate deep into the pores inherently causing plugging. The occurrence of pore blockage as a result of cake compression is to avoid since it may reflect an even more pronounced impact on fouling as compared to the external layers resistance and from this state of the membrane

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it is rather complicated to recover the filtration performance (Oh
et al., 2004). Therefore, manipulating the driving force with the
aim of regaining membrane unit efficiency is advised only with
care and membranes should be regenerated by alternative methods in order to avoid pore clogging.

437 3.4. Reactor design considerations for biohydrogen production: CSTR
438 vs. AnMBR – which way to go?

The critical assessment of the relevant, available studies implies 439 that AnMBRs are able to compete with CSTRs and both applications 440 441 can be taken into account as feasible reactor configurations for fermentative hydrogen bioproduction but perhaps for different pur-442 poses. Accordingly, it would appear that a CSTR may be slightly 443 444 better in cases when enhanced biohydrogen yields and/or specific 445 hydrogen production rates are targeted (Lee et al., 2009b; Shen 446 et al., 2009), meanwhile the alternative design of AnMBR presum-447 ably allows achieving relatively increased volumetric hydrogen 448 production rates (Lee et al., 2007). However, in some reports, the 449 overall hydrogen evolution performance of AnMBR fairly exceeds 450 that of the CSTR under steady-state operation (Kim et al., 2011; 451 Lee et al., 2008). Furthermore, AnMBRs may provide a more robust and consistent operating possibility. 452

453 Nevertheless, the selection between the two competing systems
454 should be made case-specifically since one process may fit better
455 for one particular project, while the other application can be more
456 feasible for other purposes.

Moreover, it is important that not only H<sub>2</sub> yields and production 457 458 rates as apparent key factors are to be considered when performing 459 a throughout evaluation on the systems but some additional fea-460 tures, such as downstream aspects as well. This is because an over-461 all, multi-aspect analysis of the intended process is able to change 462 the suitability of the different reactor concepts and consequently, 463 increase/decrease the relative attractiveness of CSTR and AnMBR. 464 For example, even though biohydrogen yields are not always as 465 high as in other continuous, free-cell applications, realizing an 466 AnMBR can bring some advantages such as high quality effluent 467 so that there would be no need of any complementary equipment 468 (e.g. sedimentation tank) to recycle cells or to treat the spent media. 469 Bioreactors aided with micro- or ultrafiltration membranes are able 470 to ensure a relatively clean effluent e.g. in terms of solid organic 471 matter and bacteriological parameters (Jeong et al., 2010). Hence, 472 it reduces the need and the cost of any post-fermentation processes.

However, an extensive development of the field is required to establish conclusions on more solid grounds due to the limited number of studies employing AnMBRs for biohydrogen production.

476 To facilitate the progress in AnHPMBR research, some sugges-477 tions may be given for their design, as follows: First of all, the 478 hydrogen producing inocula is of high importance. According to 479 Table 1, heat- or acid pretreated anaerobic populations would ap-480 pear to be feasible. Furthermore, it seems beneficial to get the inoc-481 ulum acclimated to a certain substrate in common bioreactors (e.g. in continuously stirred vessels) before integrating the system with 482 483 a membrane module and switching to AnMBR mode. The shifting 484 time of MBR operation should be at the point when the washout 485 of the whole cell biocatalysts becomes a potential threat in the conventional membrane-less fermenter ensuring equal hydraulic-486 and solid retention times. During AnMBR mode, the SRT/HRT ratio 487 488 is a critical process variable for hydrogen production performance. 489 The preliminary results obtained in the reactor lacking the mem-490 brane could be used as a benchmark for the ones attained in 491 AnMBR configuration. As for the membranes, microfiltration units 492 (Table 2) seems applicable but a proper operational concept is 493 needed to restrict the chance of bioreactor failures e.g. due to foul-494 ing. This claims the adequate choice of the concentration factor 495 (SRT/HRT ratio) and the permeate flux regeneration technique.

## 4. Conclusion

The present review on anaerobic membrane bioreactors – de-497 spite the limited number of relevant papers – indicates that these 498 integrated systems are attractive for biohydrogen production and 499 can be considered as alternative solutions to the most common 500 CSTR applications. However, more research dedication is needed 501 for the further development of the field e.g. to get a better under-502 standing about the interrelationship of bioreactors and t coupled 503 membranes, which is a key factor to achieve better performances 504 and a more predictable, controllable and long-term, steady-state 505 operation. 506

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