1	Electrochemical sensing with nanopores
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12	Abstract
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14	We discuss representative electrochemical nanopore sensing strategies, highlighting their
15	underlying theoretical principles, and limitations.
16	
17	Keywords
18	Nanopore sensor, resistive pulse sensing, Coulter counting, stochastic sensing
19	
20	1. Introduction
21	
22	The use of nanopores for chemical sensing generally narrows down to nanoporous
23	membranes with straight-through pores of uniform size distribution and ultimately to single
24	nanopore membranes. To understand what makes nanopores so unique in terms of their use for
25	chemical sensing we must consider the extremely small volume defined by their interior. Thus
26	species translocating or residing within a nanopore can effectively change the physical-
27	chemical properties of the nanopore interior (e.g., conductance [1, 2] or refractive index [3]),
28	which can be detected in a label-free manner. By having a single nanopore with a volume
29	comparable to that of the targeted species, detection of single species becomes feasible. The
30	use of nanopores for electrochemical sensing originates in the Coulter counter, best known for
31	blood-cell counting in hematology [4]. However, the instrumentation and implementation of
32	biological nanopores additionally benefited from studies on biological ion channels [5, 6].

Conventional Coulter counters use a single cylindrical pore to count and size particles suspended in an electrolyte. Pulsewise changes in the pore conductance are detected as insulating particles passing through replace their own volume of highly conducting electrolyte
(Fig. 1). The analytical information from a resistive pulse sensing (RPS) measurement is the
pulse height (indicative of the volume of the target), pulse frequency (proportional to target
concentration) and pulse length (depends on the mean translocation velocity and relative lengths
of the pore and the target species).

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A major strength of the method is the ability to determine particle concentration in a 41 calibration-less manner by relating the number of pulses to the known volume of suspension 42 flown through the pore. The classical apparatus detect species of ca. 2 to 60 % of the pore 43 diameter [8] and since the smallest pore diameter is 10 µm the lower size limit of the assessable 44 species is a few hundred nanometers. The reduction of the pore size is an obvious way to extend 45 the applicability of the Coulter principle to species with characteristic dimensions in the lower 46 nanometer range, e.g., nanoparticles of synthetic or biological origin, and macromolecules. 47 However, such a scaling down proved to involve essential changes compared to micropores and 48 49 to enable new detection methodologies.

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51 2. Resistive pulse sensing with single nanopores

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While in case of micropores the dominant transport form is the pressure driven flow through 53 the pore, the volume flow rates established through nanopores are orders of magnitude smaller 54 and therefore less efficient. Additionally, in case of charged species or pores the electrophoretic 55 or electroosmotic contributions, respectively, should be considered. In practice, the transport 56 through nanopores occurs through concurrent diffusive, hydrodynamic, electrophoretic, and 57 electroosmotic mechanisms resulting in a mean translocation velocity. Generally, for larger 58 diameter pores (d>10 nm) the dominant mechanism is the hydrodynamic transport owing to its 59 quadratic dependence on the pore diameter. For d < 10 electrophoresis and electroosmosis 60 dominate; with relative contributions depending on the surface charge density of the pore and 61 the translocating species. Diffusive transport scales with 1/d and becomes comparable to 62 electrophoresis only for d < 1 nm,[9] because diffusion of smaller particles is faster while 63 electrophoresis is practically independent of the pore diameter. Thus, a calibration-less 64 concentration determination is challenging with nanopores unless the hydrodynamic transport 65 prevails. In case of hydrodynamic transport while difficult to determine the minute volume flow 66 rates experimentally, they can be calculated if the pore geometry is known [10]: 67

$$Q = \frac{3\pi P}{8\eta l} \frac{d_b - d_t}{d_b^3 - d_t^3} d_b^3 d_t^3$$

where, *P* is the applied pressure η is the electrolyte dynamic viscosity, *l* is the pore length, d_b and d_t are the base and tip diameters of the conical pore geometry, respectively. Thus the pore geometry, generally cylindrical or conical, clearly plays an important role in nanopore sensing, by determining the electrical resistance, the shape of the current pulses and the overall sensitivity of the detection. The uniform cross-section of cylindrical pores results in square wave pulses, while the growing cross-section in conical pores causes an asymmetric trianglelike pulse shape [11] (Fig.1).

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2.1. Electrical resistance of nanopores

78 The general expression of the pore resistance assumes a conical pore geometry (in fact

result truncated cone) and homogeneous conductivity (valid at high ionic strengths):

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$$R_p = \frac{1}{\sigma} \int_{x=0}^{l} \frac{1}{A(x)} dx = \frac{4l}{\pi d_t d_b \sigma}$$

81 where σ is the electrolyte conductivity, x is the coordinate along the centerline, A(x) is the

cross-section at position x, d_b , d_t , and α are the base and tip diameters of the truncated cone,

and the half-cone angle, respectively $(d_b = d_t + 2\tan(\alpha)l)$.

Since the electric field lines gradually converge into the pore orifice, the changing crosssections of the ion flux can contribute significantly to the overall pore resistance. This additive component is called the access resistance (R_a) derived first by Hall [12]:

$$R_a = \frac{1}{2d\sigma}$$

88 Considering R_a at both openings the total resistance of a conical pore is

$$R = \frac{1}{\sigma} \left(\frac{4l}{\pi d_t d_b} + \frac{1}{2d_t} + \frac{1}{2d_b} \right)$$

90 while for cylindrical pores ($d_t = d_b = d$), $R = \frac{4}{\sigma d\pi} \left(\frac{l}{d} + \frac{\pi}{4}\right)$. The total resistance deviates

with only 3% from values simulated at l/d=5 using Nernst-Planck/Poisson equation, as opposed to 20% when the access resistance is unaccounted. The discrepancy is even higher for pores with lower l/d ratio.

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97 2.2. Theoretical models to estimate pulse amplitudes

During particle translocation the maximal resistance change determines the current pulse amplitude or peak height for "triangular" shaped pulses. For simplified models, such as considering uncharged pores, insulating spherical targets and translocation along the pore axis the pulse amplitude can be calculated analytically. However, in many practical cases one or more of the above assumptions is not valid and therefore numerical solutions of coupled Poisson, Nernst-Planck and Navier-Stokes differential equations [13] are used to provide the pulse amplitudes (and shapes), but at largely increased computation times.

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106 2.2.1. Cylindrical pores

There are four main models to calculate the pulse amplitude for cylindrical pores, each with 107 different validity region depending on the relative particle size (d_{part}/d) (Fig. 2.) [14]. The 108 earliest model uses the equation derived by Maxwell for the effective resistivity of a suspension 109 of insulating particles [15]. The model introduced by Gregg and Steidley treats the pore as an 110 ideal conductor containing an insulating sphere. Homogenous electric field is assumed although 111 the electric field lines distort around the particle resulting in an unaccounted resistive 112 contribution. Therefore, the model approximates the pulse amplitude from below [16]. Deblois 113 et al. assumed a "bulging" pore shape that follows the distorted electric field lines around the 114 particle. This modified shape enables to calculate the particle containing pore resistance exactly, 115 but underestimates the resistance of the empty pore by neglecting the electric field 116 inhomogeneity near the bulge. Therefore, this model provides an upper limit for the pulse 117 amplitude [1]. 118

Anderson and Quinn [17] developed the fourth model on the analogy to the numerical calculations of Smythe, who investigated the hydrodynamic resistance change in a cylinder caused by a sphere [18]. This model has the broadest validity covering the whole practically relevant particle size range (up to $d_{part} / d = 0.9$).

123

$$\frac{\Delta R}{R}\Big|_{Smythe} = \frac{1}{\left[\left(d / d_{part}\right)^3 - 0.8\right]\left(l / d + \pi / 4\right)}$$
124

$$\frac{\Delta I}{I} = \frac{-\Delta R / R}{\Delta R / R + 1}$$

where ΔR is the resistance change, *R* is the resistance of the empty pore with access terms, ΔI is the pulse amplitude.

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128 2.2.2. Conical pores

To date there is no simple analytical expression for calculation of RPS pulse amplitudes in conical pores. The main approaches to relate the pulse amplitude to the particle size and pore geometry include:

-approximation of the very end of the conical pore with a cylinder [19],

-applying the model developed by Gregg to a conical pore geometry [20],

-calibration with nanoparticles of known size and assuming that the pulse height isapproximately proportional to the particle volume [21].

These approaches are valid only at sufficiently high electrolyte concentrations because the number of counter ions shielding the surface charge of the nanopore [22] or the analyte [23, 24] should remain negligible in the pore interior with respect to the free ions of the electrolyte. The resistance calculations also assume continuum media which is valid until the smallest dimension of the pore is larger than 10 nm [25].

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142 2.3. Noise during RPS measurements

After electrical shielding RPS measurements are affected by ΔI_T thermal noise stemming from the thermal motion of charge carriers, the ΔI_D dielectric noise due to the energy dissipated by the dielectric pore substrate, the ΔI_A amplifier noise generated by the headstage and the ΔI_F flicker (or 1/f) noise, arising only when voltage is applied. [26, 27] These noise components are independent and the total noise level is:

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$$\Delta I_{total} = \sqrt{\Delta I_T^2 + \Delta I_D^2 + \Delta I_A^2 + \Delta I_F^2}$$

The noise is attenuated by electrical shielding, analog/digital noise filtering and using low-149 noise/low-capacitance materials for the nanopore membrane. The bandwidth of the 150 measurement can influence both the noise level and the shape of the current pulse. While a high 151 bandwidth increases the noise, a bandwidth lower than the highest frequency component of a 152 translocation pulse results in signal attenuation/distortion. Considering this trade-off the cut-off 153 frequency during RPS experiments is generally 10 kHz. Commonly, thermal noise dominates 154 when R is less than ca. 10 M Ω , while at ca. 100 M Ω resistance and 20 kHz cut-off frequency 155 the amplifier and dielectric noise also become comparable. Above 100 M Ω pore resistance 156

usually amplifier or dielectric noise sets the total noise level while the flicker noise is typicallynot dominant because of signal filtering.

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160 2.4. RPS for selective detection

Solely size and shape information are not sufficient to identify target species in a complex 161 matrix. Therefore, selective receptors either immobilized to the nanopore environment or added 162 to the sample solution have been used to induce target-specific changes in the RPS signal. 163 Selective receptor is added to the sample generally to increase the size of the target species and 164 consequently the pulse amplitudes. This principle is illustrated in Fig. 3A through selective 165 detection of viruses by adding capsid-binding antibodies into the sample [28]. An alternative 166 approach is to monitor the translocation of a receptor the conformation (size) of which is altered 167 upon binding the target species. A relevant example is the detection of cocaine through the 168 blocked translocation of the cocaine-specific aptamer, which suffers a conformation change 169 upon cocaine binding that prohibits its translocation through the pore [23]. Using solid-state 170 nanopores through which double-stranded DNA strands translocate, but not their complexes 171 with restriction enzymes, allowed the identification of single-nucleotide polymorphism by 172 detecting the increase in the threshold voltage, i.e., the minimum voltage required to drive the 173 DNA strands through the nanopore by releasing the restriction enzyme[29]. 174

In the simple case of having immobilized receptors that on the time scale of the analysis bind their target reversibly with 1:1 stoichiometry the pulse duration can be related to the dissociation rate constant (k_{off}) of the analyte-receptor complex:

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$$\Delta t = \frac{1}{k_{off}}$$

The mean time between successive binding events is a function of both the concentration and the association rate constant (k_{on}) [30]:

 $\Delta t_{on} = 1/k_{on} c$

Thus, for selective stochastic sensing low affinity receptors can be used bot for quantitative determination of the target as well as to determine the kinetics of single molecule binding events [31, 32]. In case of "irreversible" target binding permanent blockage events are observed [32, 33], which can be used for a "Yes-No" type identification of a given species. Quantitative detection is also feasible by measuring the mean time elapsed until the target binds to the receptor, which is inversely proportional to its concentration [33]. In the case when the single nanopore possess multiple binding sites (Fig. 3B), characteristic to receptor functionalized solid-state nanopores, the time elapsed between the first and second binding can be used as a more convenient modality for quantitative analysis [34]. Multipore membranes can be also used for quantitative sensing, in which case a cumulated change of the membrane resistance is detected, without the possibility to differentiate single binding events [35].

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194 2.5. Detection limit of RPS

While RPS has single species detection capability, as the signal is due to individual species translocating through the nanopore, the detection limit is in fact determined by the target throughput. At low concentrations the probability of a species encountering the pore becomes very small; the limiting situation being the undirected, Brownian motion of a single particle in

a volume V, that requires a mean encounter time of $t_e = \frac{V}{2Dd}$ (D is the diffusion coefficient of 199 the target) [36]. Thus, in RPS the translocation frequency decreases with the analyte 200 concentration, but for statistical analysis there is an f_{event}^{min} minimal frequency that results in a 201 practical measurement time (e.g. 100 pulses in 10 minutes). It is possible to increase the event 202 frequency (e.g. by applying hydrostatic pressure), but at the expense of a higher translocation 203 velocity, that shortens the duration of the current pulse. Shorter pulses than the electronic filter 204 rise time τ_{rise} , will be attenuated and thus useless for analyte sizing. The salt gradient method 205 used by Wanunu et al. is to date the only approach to simultaneously boost translocation 206 throughput and increase translocation time [37]. 207

Assuming that the flux of target species is the constant through every cross-section of the analyte flow, c_{min} can be introduced as the minimal concentration, which is measurable without significant attenuation of the pulse amplitude:

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$$c^{\min} = \frac{1.36}{d^2 \pi l_{rise} N_A} \frac{f_{event}}{f_c^{\max}}$$

where *d* is the diameter of the pore orifice (the tip diameter for conical pores), N_A is the Avogadro-constant, f_c^{max} is the maximal cut-off frequency where the analyte is still detectable irrespective of the current noise. The parameter l_{rise} is the distance between the analyte positions where the current pulse starts to deviate from the baseline and where it starts to deviate from the peak value (Fig. 4). The approximations $l_{rise}^{cyl} = d_{part}/2 + l$ for cylindrical, 217 $l_{rise}^{cone} = \frac{d_{part}}{2}$ for conical geometries were used with $\tau_{rise} = \frac{0.34}{f_c}$ as typical in RPS

218 measurements [7].

Larger pores require lower analyte concentration because the detection limit scales inversely with the pore volume (cylindrical pores) or with the third power of the tip diameter (conical pores). According to Fig. 4 the detection limit of cylindrical pores is always lower than of conical pores at equal pore/tip diameters. Generally, this is not true because conical pores are more sensitive than cylindrical pores that enables to use a wider orifice for the same particle size.

225

226 **3. Potentiometric sensing**

Owing to the small diameters of nanopores the chemical-physical properties of the surface can 227 selectively alter the transpore flux of ions through the nanopore (Fig. 3C). An early 228 potentiometric study showed that membranes with charged nanopores rejected ions of the same 229 charge sign and transported those of opposite charge [38]. The potentiometric response of such 230 permselective nanopores can be described well by using the Nernst-Planck/Poisson equations 231 [39]. Further increasing the transport selectivity of the nanopores by restricting it to a single ion 232 is possible by using a selective complexing agent (Ag⁺ ionophore) and a hydrophobic 233 compound grafted to surface of the nanopore, in addition to ion-exchanger sites. Simple 234 potentiometric measurement of the membrane potential resulted in Ag⁺ -selective electrodes 235 with nanomolar detection limit and selectivity coefficients exceeding six order of magnitudes 236 for common ions [40]. 237

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243 **5. References**

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295 Figure captions

296

Fig. 1. Schematics of a single nanopore sensor (left) and typical current responses for cylindrical and conical pores (right). The ionic current through the nanopore is maintained by applying a transmembrane voltage between two Ag/AgCl electrodes. The full width at half maximum (fwhm) is a measure of the pulse duration while ΔI of the pulse amplitude [7].

301

Fig. 2. Relative current changes calculated with different models in a cylindrical pore with l/d=20 as a function of the relative particle size. Regions in brackets indicate approximate validity range of the models.

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Fig. 3. Schematics of nanopore sensing methods and resulting signals. (A) RPS measurement

with a selective reagent added to the sample, (B) analyte binding by a functionalized nanopore,

- 308 (C) nanopore-based ion-selective membrane.
- 309

Fig. 4. Detection limit for particle sizing as function of pore diameter for a conical pore and

cylindrical pores with various lengths ($d_{part} / d = 0.5; f_c^{max} = 10 \text{ kHz}$).



Figure 2 Click here to download high resolution image



Figure 3 Click here to download high resolution image



Figure 4 Click here to download high resolution image

