

Radon emission evolution and rock failure

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Received: 2 June 2015 / Accepted: 17 October 2015 / Published online: 28 October 2015
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Abstract Previous experimental studies showed that the variation of Radon (Rn) emission is closely related to the development of rock deformation: Rn emission has a rapid increase with the growth of cracks and their surface areas (i.e. onset of fracture coalescence point), and reaches the maximum at rock failure. In this study, the stress level at the onset of fracture coalescence λ_c is predicted with the renormalization group theory. It is assumed that rock is a strain-softening medium whose strength can be described by Weibull's distribution. Result shows that λ_c depends mainly on the homogeneity index or shape parameter m in the Weibull's distribution for the rock. Both experimental and analytical results show that this point of rapid increase in Rn emission on the Rn-strain curve corresponds to the critical point on the stress-strain curve; for rock compression, the stress at this point is approximately 70–80 % of the peak strength. Hence a generalized crack damage threshold is proposed in the present study based on the characteristics of Rn emission during the loading process, for recognizing the critical point of rock fracture.

Keywords Rock failure · Critical information · Rn emission · Identification

1 Introduction

Studying the mechanical behavior of rock failure based on its stress-strain curve and other physical parameters has important scientific and engineering values (Chen and Lin 2004). Variation of rock cracking or porosity under an external load can affect the rock's stress-

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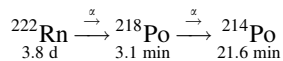
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strain state and other physical parameters (i.e. ElectroMagnetic emission energy (EME), Dou et al. 2007), velocity (Chen et al. 1990), and resistivity (Figs. 1, 2, 3), and variations in these parameters can reflect the development of rock failure. From Figs. 1, 2 and 3, it is easy to see that the EME, velocity, and resistivity have significantly changing at point C (roughly corresponding to the yield point).

The fracturing of stressed materials is analogous to the critical phenomenon at a second-order phase transition or the percolation phenomenon (Herrmann and Roux 1990; Sornette 2000). The moment of rupture can be regarded as a critical point, so the fracturing process can be described with a renormalisation-group scheme (Anifrani et al. 1995). In a region in the vicinity of the critical point of rupture (Sornette and Andersen 1998), the variations in free energy, which is reflected in the released energy, can be characterised by a power law decorated by log-periodic oscillations (Sornette 1998).

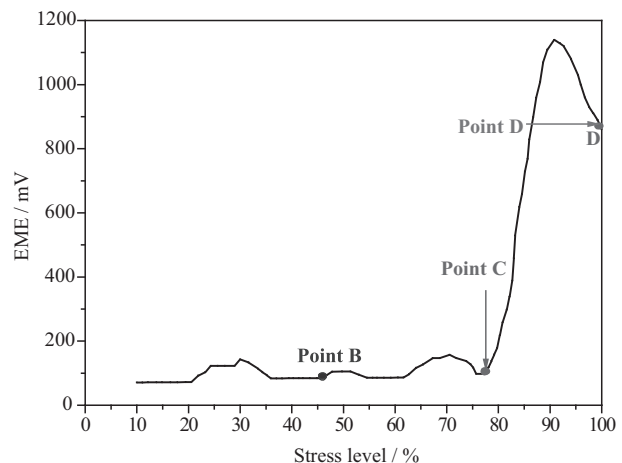
In this study, we select the Rn emanation of rock as the internal variable, and three parameters, “stress level (normalized relative to the compressive strength), strain level (normalized relative to the axial strain threshold at the uniaxial compressive strength) and Radon emanation density”, are used in the measurement and the state equations of rock. Rn is the only radioactive gas in nature. Its radioactivity comes from the following reaction



The radioactivity of Rn is related to its atomic mass, atomic number and ionization energy. Rn has the largest atomic mass and atomic number among the six rare gases (i.e. He, Ne, Ar, Kr, Xe, and Rn), but the lowest ionization energy, as shown in Fig. 4. It is widely distributed in nature, i.e. in all kinds of rock, gypsum, concrete, sand, and water. In rock, Rn exists in three forms, including freedom, adsorption and sequestration (Wang 1990, 2010).

In most geological hazards (e.g. earthquake, landslide, rock collapse and inrush of coalmine), the development of cracks in rock plays an important role. Variations in Rn emanation have been considered as a possible precursory phenomenon for evaluating the deformation and fracture feature of rocks (Zhou et al. 1981). Significant achievements have been made in systematic studies on the variation of Rn emission with rock cracking (Luo

Fig. 1 Variation of electroMagnetic emission energy (EME) during pre-peaking phase of raw coal in Dongtan Mine (Dou et al. 2007)



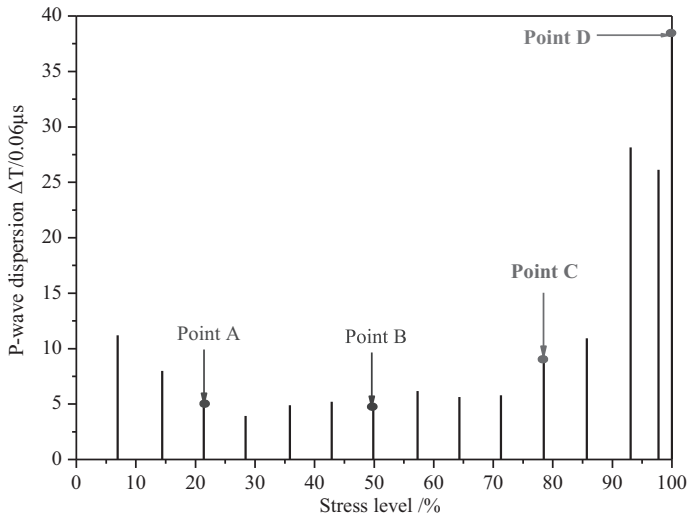


Fig. 2 Relationship between travel times of P-wave versus stress level in marble sample (Chen et al. 1990)

and Shi 1980; Holub and Brady 1981; Luo et al. 1981, 1984; Kies et al. 2005). Holub and Brady (1981) pointed that a generating mechanism of the Rn concentration anomalies in the co-seismic rupture was possibly enlargements of effective area of grain surface, porosity and radon emanation rates, which resulted from co-seismic cracking of rocks. Increase of Rn emission was found to generally start when the applied stress reaches 20–90 % of the corresponding failure stress, probably caused by the occurrence and growth of dilatant microcracks in rock (Zhou et al. 1981), which leads to increased emanation (King and Luo 1990). Kies et al. (2005) also proposed that variable volumetric strain and stress had important influence on the radon concentrations. Detecting the variation of Rn emission has been used in disaster geology (Wang 2010) and predicting earthquakes (Luo et al. 1984; Li et al. 1984; Crockett et al. 2006; Zhou et al. 2010).

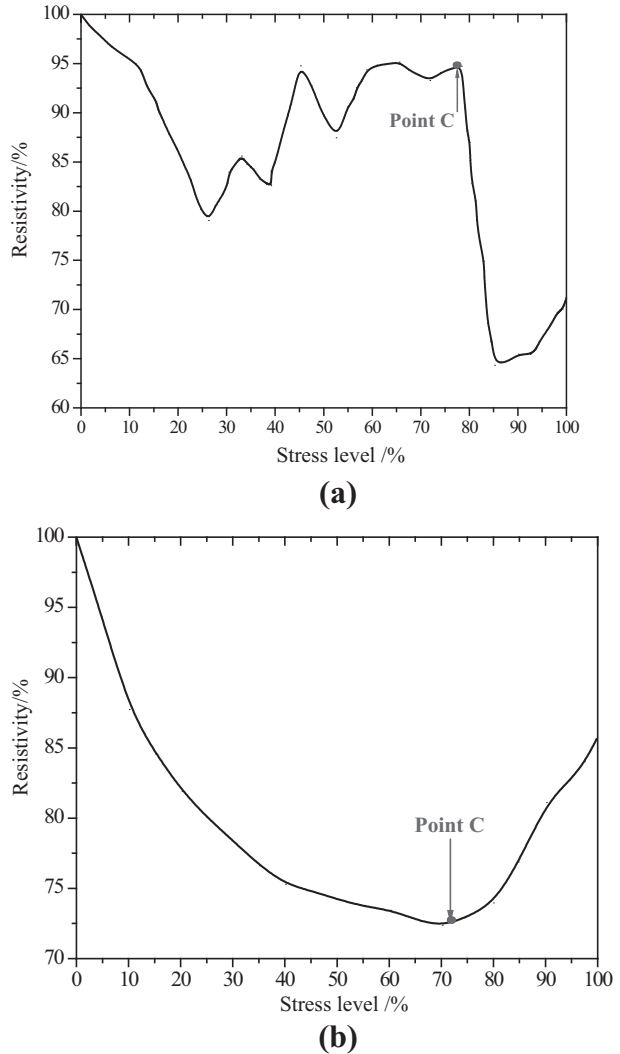
This paper is a generalization and extension of previous studies. In this study, based on fracture mechanics, we introduce a few key concepts for understanding the evolution of Radon emission at a critical point on the stress–strain curve, and develop a renormalisation-group method to indirectly predict the occurrence of rock fracture.

2 Rn emission evolution and stress–strain of intact rock under compression

Rocks inevitably contain pores, flaws or microcracks. For example, weak grain boundaries may serve as sources of cracking. Microcracks will grow when the rock is loaded beyond a certain threshold, which is also reflected in the evolution of Rn emission.

Several characteristic stress levels identified in laboratory tests are important to understanding the failure of rock. They are shown as the stress–strain relation in Fig. 5: σ_a is the crack closure stress level; σ_b is the crack initiation stress level; σ_c is the crack damage stress level corresponding to long-term rock strength (Martin 1993, 1997) (i.e., the critical stress level), and σ_d is the peak stress. Rn emission events start to increase at σ_b and

Fig. 3 Relationship between resistivity and stress level.
a Sandstone 2# (Lu et al. 1992);
b No. 8 coal petrography (Li et al. 1999)



increase drastically when σ_c is reached. The maximum Rn emission is usually reached near σ_e , which is at the turning point of the constitutive curve. Three stress levels σ_b , σ_c , and σ_d , represent important stages in the development of macroscopic failure of intact rock (Martin 1997; Cai et al. 2004; Xue 2011).

The following characteristics of microcracking, Rn emission and rock failure have been found in previous studies:

- (1) Rn emission increases at stress levels approximately 0.3–0.5 times the peak uniaxial load (Figs. 5, 6, 7).
- (2) Microcracks form or propagate mainly in the direction parallel to the maximum compressive stress. This is evident from the measured volumetric strain dilatation (Martin 1997) and direct microscopic observation of test samples.

Fig. 4 Atomic weight and atomic number versus ionization energy of rare gases

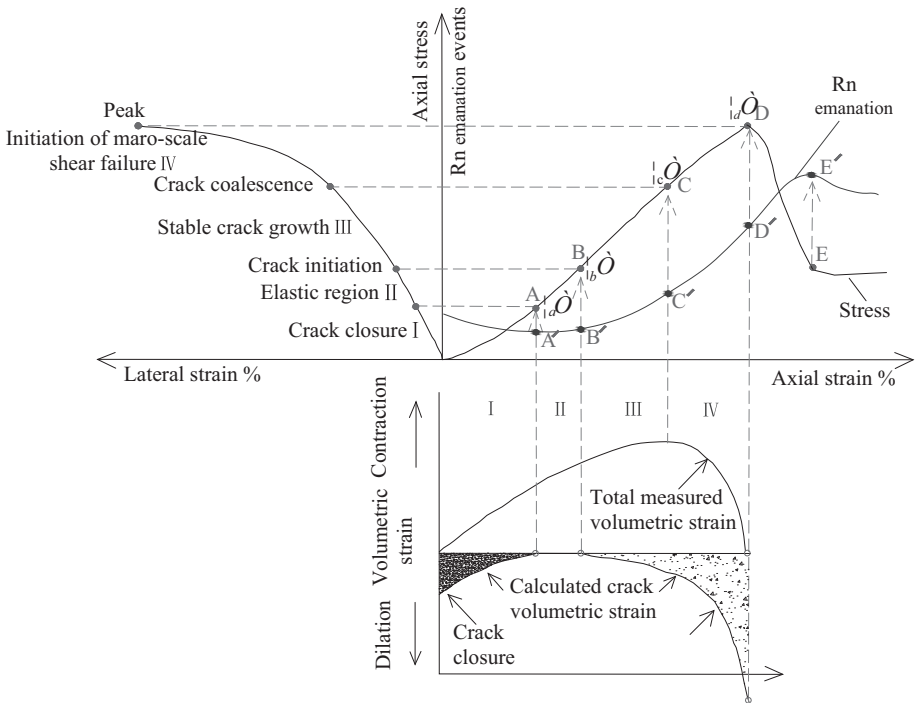
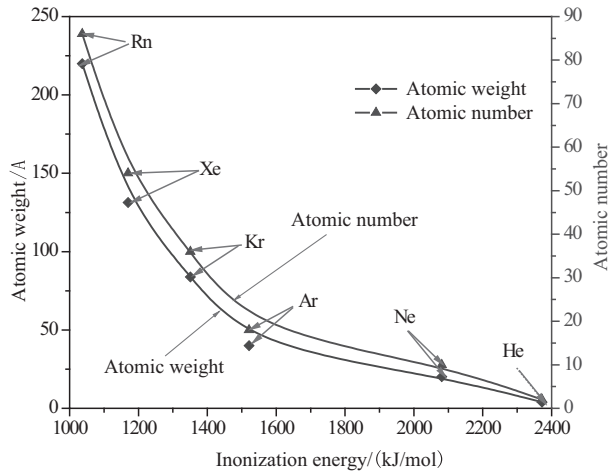
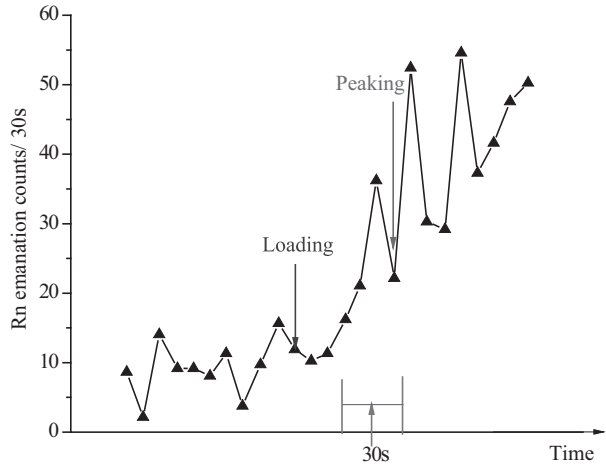


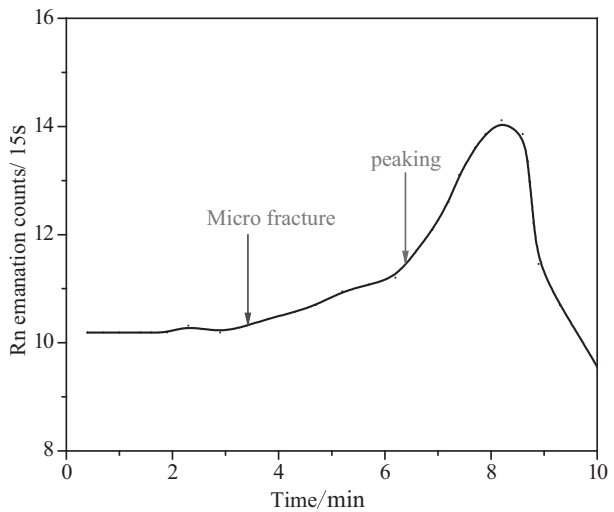
Fig. 5 Stress–strain diagram showing the stages of crack development by Rn emission [after Martin et al. (2001) and Cai et al. (2004)]

- (3) Onset of fracture coalescence starts at stress levels approximately 0.7–0.8 times the peak strength (Lockner et al. 1992).
- (4) Macrocracks or shear bands normally form after the peak strength is reached.

Fig. 6 Relationships between Rn emanation versus time in the loading process of rock materials. **a** The impact of loading to Rn emission (Luo et al. 1981). **b** Results of pressure related Rn experiment with no water (Li et al. 1984)



(a)



(b)

Based the Rn emission change versus stress level (Figs. 6, 7) obtained from experiments on rock samples, the variation of Rn emission with stress level can be separated into 3 phases. (1) In the compaction and elastic phases, there is a mixed trend in Rn emission with the increasing of stress. The Rn emission starts increasing at Point B, when stress level reaches 30–60 % of the peaking stress. (2) After the point B, with the increase of loading, micro cracks appear and gradually expand. In this process, the Rn emission increases. (3) Nearly to the Point C, plenty of micro cracks initiate and grow rapidly, and micro breaking is developed spatially in rows along the potential breaking planes until the microcracks eventually become connected with each other (Figs. 6, 7, 8), as indicated by the

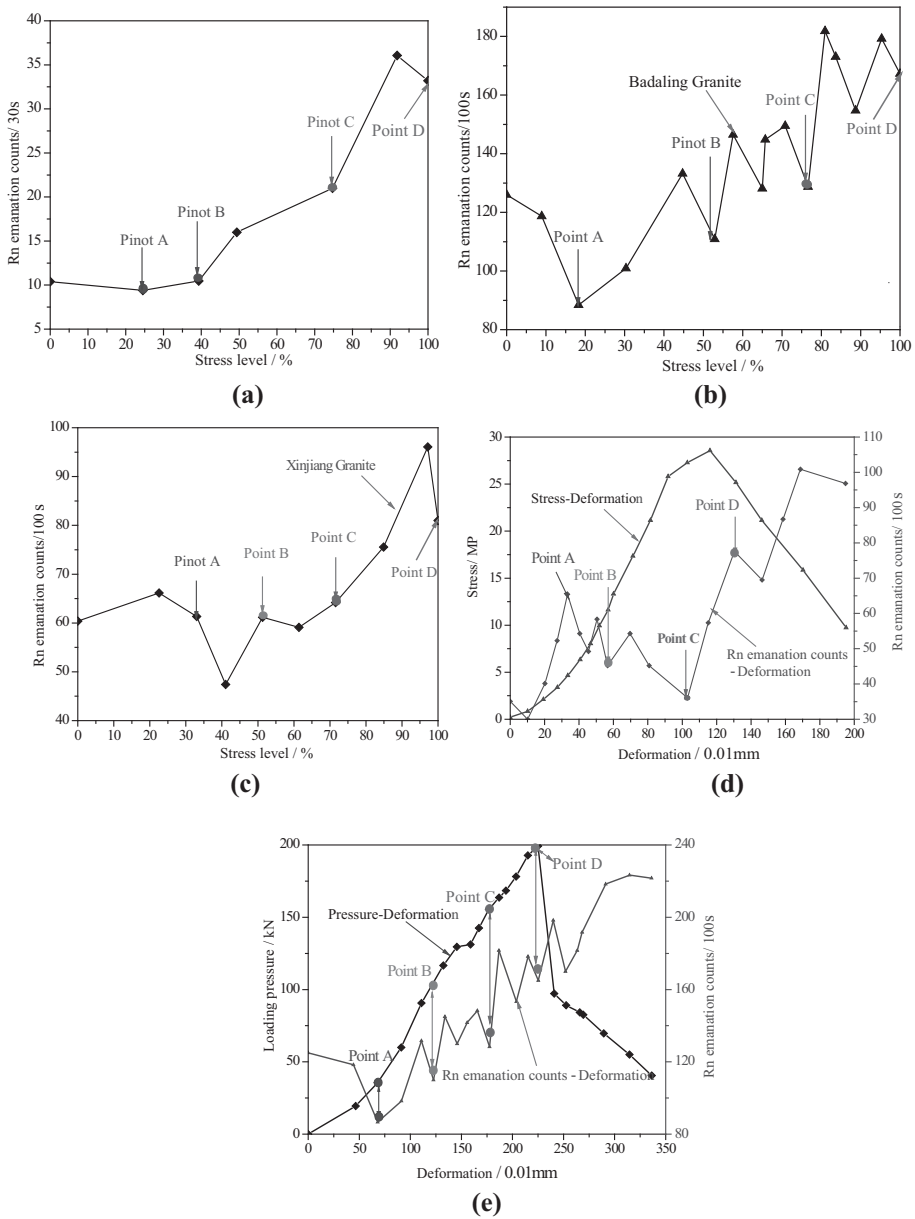
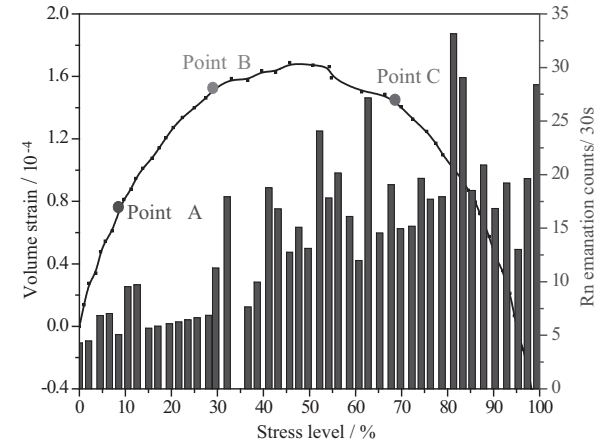


Fig. 7 Relationships between Rn emanation versus stress level during loading process. **a** Concrete (Luo et al. 1981); **b** badaling granite (Luo et al. 1981); **c** granite (Luo et al. 1981); **d** concrete (Luo et al. 1981); **e** badaling granite (Luo and Shi 1980)

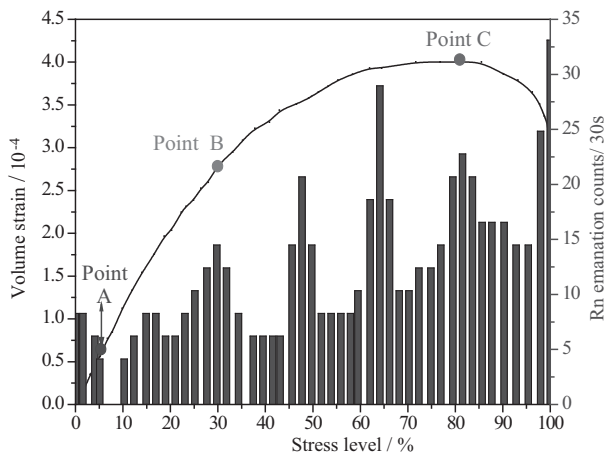
localization of strain, and accelerated increase of volumetric strain at the cracks. In this phase, the Rn emission is increasing steeply.

Rn emission generally increases with the growth of cracks. In laboratory tests, σ_b (the crack initiation stress or threshold) is defined as the onset of stable growth of cracks, or the

Fig. 8 Relationships between Rn emanation versus stress and average volumetric strain versus stress level in loading process of concrete (Zhou et al. 1981). **a** No. 4, **b** No. 5



(a) No.4



(b) No.5

stress level when crack volumetric strain deviates from zero. In some cases, testing samples may have been damaged in the course of preparation, so Rn emission can be detected at the crack closure stage. For this reason, Rn emission events recorded during the crack closure must be subtracted from the total cumulative count to avoid confusion in data analysis, when accumulated Rn emission counts are used to study the crack initiation and crack damage stress levels (Fig. 8).

The crack damage stress is generally defined as the stress level when volumetric strain reversal occurs and unstable growth of crack begins. Rn emission increases with the growth of pore surface during rock failure (Wang 2010). Under the vibration condition, Rn emission increases drastically, as shown in Fig. 9 (Luo et al. 1984). Existing cracks start to propagate and new cracks initiate in a stable fashion when the damage initiation limit is exceeded, but critical rock mass damage is only encountered when crack density is sufficient for cracks to coalesce and form shear band or tensile spalls. This state is defined as

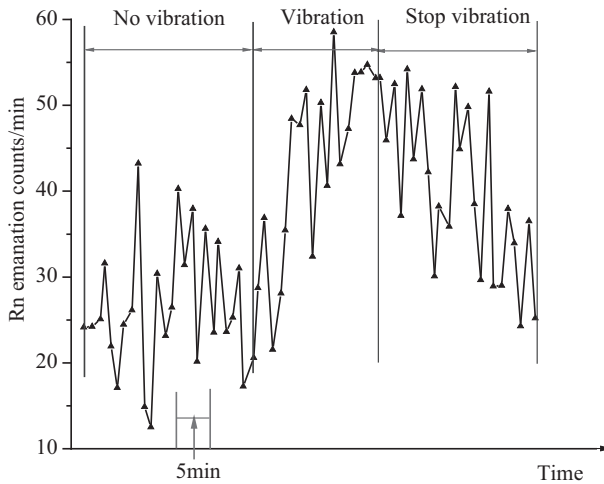


Fig. 9 Relationships between Rn emanation versus time in the vibration process of Liaoxi granite (Luo et al. 1984)

the “crack damage stress” (Martin 1997) or “Rn emission damage threshold” because in general, a single Rn emission can be viewed as a cracking event. Therefore, the crack damage stress also corresponds to the stress when drastic increase of Rn emission activity (the slope of the accumulated Rn emission events increases sharply) is observed.

In laboratory tests (Xue et al. 2014a, b), the crack damage stress level σ_c increases with the level of confinement. Hence, the unconfined σ_c determines the onset of failure propagation process in the field. In other words, σ_c can be considered as the “wall rock strength” in massive rocks. Table 1 summarizes some of the crack initiation and crack damage stress levels obtained from uniaxial and triaxial compression tests. In triaxial tests, the stress levels are defined by the deviatoric stress ($\sigma_1 - \sigma_3$). It can be found that the σ_b/σ_d ratio varies between 32 and 54 % and the σ_c/σ_d ratio varies between 70 and 81 %.

3 Prediction of the probability of critical rock failure

Table 1 shows that the measured stress level at the threshold point of destruction C ranges from about 70 to 80 % for most samples. In this section, we develop a theoretical method to indirectly predict the probability of critical rock failure.

Table 1 Summary of crack initiation and crack damage stress levels from laboratory test by Rn emission

Rock type	σ_b/σ_d (%)	σ_c/σ_d (%)	References
Concrete	32.1	81.0	Zhou et al. (1981)
Concrete	30.9	70.1	Zhou et al. (1981)
Concrete	39.3	74.5	Luo et al. (1981)
Badaling granite	44.7	76.7	Luo et al. (1981)
Xinjiang granite	41.1	71.6	Luo et al. (1981)
Badaling granite	54.1	78.7	Luo and Shi. (1980)

Based on the Weibull distribution, Qin et al. (2008, 2010a, b) used the classical Weibull's distribution to represent the probability p_x that the failure strength σ_f of a block is less than the stress $\alpha\sigma$

$$p_x = p(\sigma_f < \alpha\sigma) = 1 - \exp\left[-\left(\frac{\alpha\sigma}{\sigma_0}\right)^m\right], \quad (1)$$

where σ is stress; α is the scale parameter; σ_0 is a measurement of average strength; and m is the shape parameter, a measurement of the variability of rock strength.

The failure probability of elementary blocks corresponding to $\alpha = 1$ can be expressed as

$$p_1 = p(\sigma_f < \sigma) = 1 - \exp\left[-\left(\frac{\sigma}{\sigma_0}\right)^m\right] \quad (2)$$

Combining Eq. (1) with Eq. (2), one has

$$p_x = 1 - (1 - p_1)^{\alpha^m} \quad (3)$$

The conditional probability $p_{a,b}$ that failure will occur (Allegre et al. 1982) when the stress $(a - b)\sigma$ is transferred to an unbroken block supporting a stress $b\sigma$, can be written as

$$p_{a,b} = \frac{p(b\sigma < \sigma_f < a\sigma)}{p(\sigma_f > b\sigma)} = \frac{P_a - P_b}{1 - P_b} \quad (4)$$

If critical damage phenomenon exists in the loading process of rock, then the failure probability $P^* = f(m)$ can be expressed as

$$f(m) = P^* = 1 - 0.5^{\frac{1}{2^m - 1}} \quad (5)$$

Equation (2) could be expressed as a probability function of strain, that is,

$$P = 1 - \exp\left[-\left(\frac{\varepsilon}{\varepsilon_0}\right)^m\right], \quad (6)$$

where, ε is the axial strain of the rock and ε_0 is the average strain.

Here, the stress–strain constitutive model of the rock can be expressed as:

$$\sigma = E_0\varepsilon \exp\left[-\left(\frac{\varepsilon}{\varepsilon_0}\right)^m\right], \quad (7)$$

where E_0 is the initial elastic modulus. By solving the first derivative for Eq. (7) with respect to the stress ε , the strain value corresponding to the peak strength is

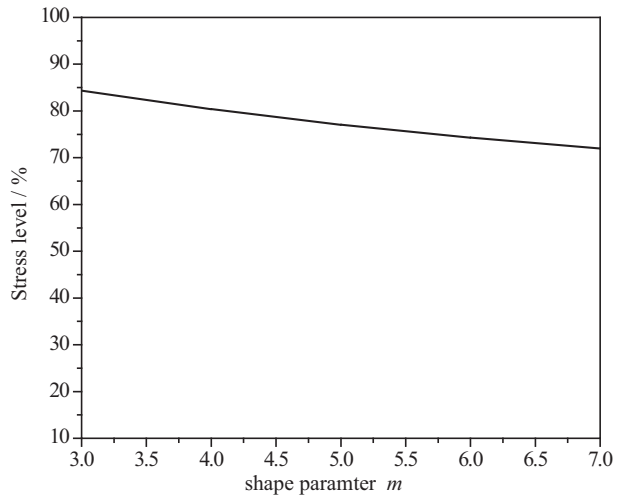
$$\varepsilon_d = \left(\frac{1}{m}\right)^{1/m} \varepsilon_0 \quad (8)$$

Substitute (2) into Eq. (8), then the strain at the critical failure point C can be written as

$$\varepsilon_c = \left(\frac{\ln 2}{2^m - 1}\right)^{1/m} \varepsilon_0 \quad (9)$$

Divide Eq. (9) by Eq. (8), then we have

Fig. 10 The variation of the critical stress level with the shape parameter



$$\lambda_c = \frac{\sigma_c}{\sigma_d} \times 100 \% = \left(\frac{m \ln 2}{2^m - 1} \right)^{1/m} \exp \left[\frac{1}{m} - \frac{\ln 2}{2^m - 1} \right] \times 100 \% \quad (9)$$

The relationship between stress ratio of σ_c/σ_d and shape parameter m is shown in Fig. 10.

This renormalization group probability of destruction is then employed to calculate the stress at the threshold point and the stress corresponding to the peak strength, which are shown and compared with the experimental results in Table 1. The predicted onset of fracture coalescence occurs at stress of approximately 70–80 % times the peak strength, agreeing with the statistical mean of the range of stress level for sharp increase of Rn emission collected from laboratory samples. Hence, Rn emission could be used to identify the range of critical point C in the stress–strain curve.

4 Conclusions

Investigating the crack damage in rocks by fracture mechanics and statistical physics, we found that the stress at critical point on the stress–strain curve is closely related to the point of rapid increasing on the Rn emission. We can use the variation of Rn emission to obtain the end stress of rock elastic stage (corresponds to point B), threshold point (corresponds to point C) and poisson's ratio.

We define σ_c and σ_d as the critical stress and peaking stress, and λ_c as the critical stress level of σ_c/σ_d . The predicted critical stress is approximately 70–80 % times the peak strength, agreeing with the statistical mean of the range of stress level for sharp increase of Rn emission collected from laboratory samples.

Hence a generalized crack damage threshold is proposed in the present study based on the characteristics of Rn emission during the loading process, which can be used as an internal variable characterizing the information on porosity change and information source to recognize the critical point of rock failure.

Acknowledgments This research was supported by the State Basic Research and Development Program of China (No. 2013CB036003), the Priority Academic Program Development of Jiangsu Higher Education Institutions, Transport project of China (2013318J12330) and the National Science Youth Foundation of China (41102201).

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