

A METHODOLOGY FOR THE DEVELOPMENT OF HISTORICAL BUILDING ARCHETYPES FOR SEISMIC PERFORMANCE ASSESSMENT

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Abstract: The probabilistic estimation of the magnitude of historical earthquakes requires the analysis of actual building structures affected by those earthquakes. The analysis complicates because most of these buildings no longer exist or were greatly modified, present a great variety of features and the number of analysis for probabilistic assessment is high. As it is not practical to analyze all structures, an alternative is to use structural archetypes representing the affected buildings. This paper presents an approach to develop a quantitative framework for the generation of historical archetypes. The method is illustrated via the definition of a specific archetype for the study and assessment of the effects of the 1763 Komárom earthquake. The historical survey of Tata, Hungary, is assumed as representative of the region and one historical building is utilized to illustrate the archetypes evaluation process.

Keywords: Structural archetype development, 1763 Komárom earthquake, Historical architecture, Historical building survey, Probabilistic earthquake magnitude assessment

1. Introduction

The great majority of seismic events occurred long before the advent of modern seismology (20th century onwards). Therefore, seismologists often engage in considerable efforts to study the macro-seismic effects of historical earthquakes in order to characterize the seismicity of a given region. This is particularly important in regions with low to moderate seismicity, as in Hungary, where the number of seismic records to perform seismic dynamic analysis of new buildings is scarce, as can be seen in [1]. The most common techniques used by seismologists, after the evaluation of the macro-seismic effects, rely on the Modified Mercalli Intensity scale (MMI) to provide intensity

point(s) [2], [3]. Afterwards, they use empirical relationships relating magnitude with either the epicentral intensity or radius to achieve the magnitude estimates. This process greatly simplifies the issue of the structural behavior of the buildings affected by the earthquake. An alternative approach considers the structural nonlinear behavior, relying on structure specific fragility functions, and uses the background of Probabilistic Seismic Hazard Analysis (PSHA) for magnitude estimation [4]. In turn, fragility functions can be achieved either by experimental laboratory tests or by analytical tools, with the Capacity Spectrum Method (CSM) [5] or Dynamic Structural Analysis (DSA) [6], [7], which require the structural modeling of the buildings damaged by the historical earthquake in study. This study is complicated by the fact that most of these buildings do not exist anymore, or were considerably modified, making them unsuited for analysis. An alternative solution is to create structural archetypes representing the affected building environment. Therefore, in order to create the structural archetypes, the framework must incorporate regular geometrical and mechanical properties so that the seismic behavior of the archetypes can be associated to that of the buildings affected by the earthquake.

The present paper focus on the development of structural archetypes for the estimation of the magnitude of the historical earthquake of Komárom, occurred in 1763. The method uses buildings of interest selected from the historical building survey of Tata [8] - due to the proximity and similar architecture - to create a numerical framework of geometrical parameters and indices [9], [10] providing the bounds in which the archetype is generated. In turn, the form of the archetypes is provided either by bibliography or abstraction from the historical analysis of the surveyed buildings. The use of the indices should guarantee the equivalence between the seismic behavior of archetypes and real buildings.

2. Probabilistic magnitude estimation methodology

A new method providing magnitude estimates based on the seismic damage analysis of historical buildings [4] (*Fig. 1*) triggers a considerable shift in the field of historical earthquake research, as the discussion is no longer prone just to the cooperation between seismologists and historians [11] but also to earthquake engineers and architect historians.

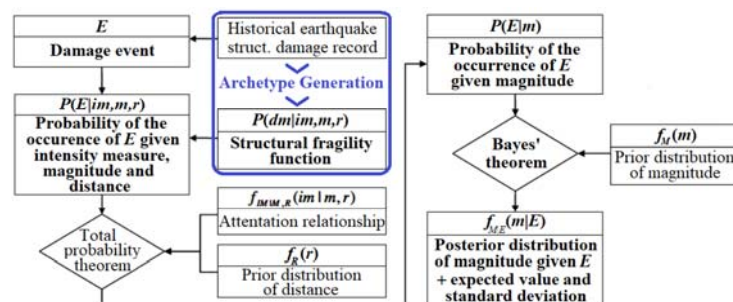


Fig. 1. Present scope in the flowchart of the magnitude estimation method, on the basis of [4]

An application of the method for the 1763 Komárom earthquake, proposed and explored in [4] (*Fig. 1*), is illustrated here in order to highlight the relevance and aim of the historical archetypes. This application example is detailed in [12] and makes use of the processes developed in [13]. Despite the correct use of methodology, the reliability of the final magnitude estimates is still conditioned by uncertainties related to the model, strength parameters and to the quantification and relation of the building/damage pairs.

2.1. Fragility functions

The fragility functions $P(dm_i|im,m,r)$ were generated with the help of a nonlinear spring model calibrated for the walls of an archetype (*Fig. 2*, left) and subjected to ground acceleration records. The algorithm was written for Incremental Dynamic Analysis (IDA), a DSA technique, for which the PGA is gradually scaled until the collapse of the structure (*Fig. 2*, center). This process enables the determination of the damage points associated with the damage states dm_1 to dm_4 [12], to which lognormal CDFs, or fragility functions (*Fig. 2*, right), are fitted. These are used in the magnitude estimation procedure (*Fig. 1*) to estimate the probability of a damaging event $P(E|im,m,r)$ which is achieved by combining the fragilities with the number of buildings under damage states $n_k=[dm_0 \dots dm_4]=[105 \ 44 \ 42 \ 35 \ 27]$, fractions of the total number of damaged structures [14], [15].

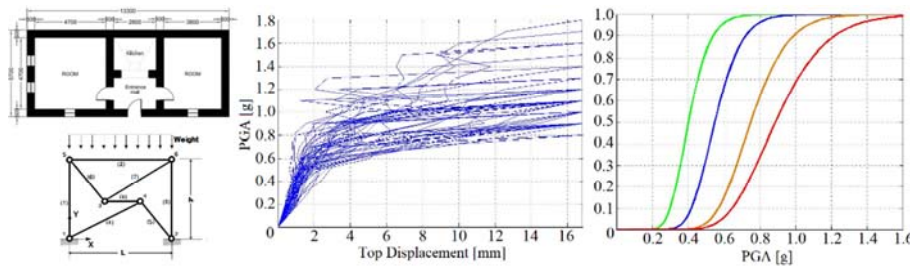


Fig. 2. Archetype 'A0' and structural model (left), IDA analysis (center) and respective fragility functions (right), on the basis of [13]

2.2. Magnitude estimation

The probability of the event given a magnitude $P(E|m)$ is calculated using the total probability theorem, by integrating the probability of the damaging event E , $P(E|im,m,r)$, together with the attenuation relationship ($f_{im|m,r}$, *Fig. 3*, centre) [16] and distribution of distance (f_r , *Fig. 3*, left, with $r_u=20$ km). Afterwards the Bayes' theorem used a uniform prior distribution of magnitude (f_m) to calculate the posterior distribution of magnitude and a magnitude expected value of 6.5. Even though, a key point in the methodology, before the calculation of the fragilities, is to input the historical earthquake structural damage record providing the number of structures of a given type under different damage states. In this case, a structural archetype of peasant house was

arguably assumed, based on expert judgment. Although, archetype should also be endorsed by both the literature and historical sources, and the historical survey of the buildings of interest.

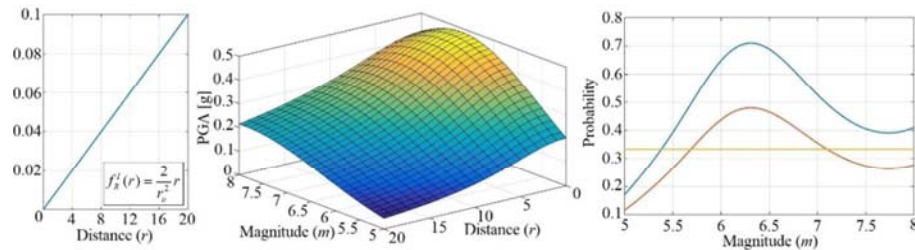


Fig. 3. Distance distribution (left), median PGAs (center) and magnitude PDF and CDF (right)

3. Historical damage sources and magnitude estimates

The 1763 seismic event, with epicenter near Komárom, was one of the strongest and most destructive in Hungarian history (*Table I*). It occurred before the instrumental era in seismology, 8 years after the 1755 Lisbon earthquake, when European institutions started regarding earthquakes as a natural hazard, rather than a product of sin, which rapidly led to the production of books [17], documents [18], depictions (*Fig. 4*) and oral descriptions.



Fig. 4. Buildings affected by the 1763 Komárom earthquake: anonymous depiction (left), depiction by Karl Friedl (right)

3.1. Later sources and magnitude estimates

The production of later sources related to the 1763 earthquake is both scientific and popular, edited into periodicals and books. The founding remark in seismology was written in Réthly's *The Earthquakes of the Carpathian Basin* [19] with antecedent in the 18th century *Dissertatio de Terrae Motibus Regni Hungariae*, by János Grossinger [17] an eye-witness of the event. The work sourced the later characterization of the regional seismicity [14], [20]–[22]. The magnitude is currently estimated in between 5.7 [23]–[25] and 6.5 [15] (*Table I*). This gap is due to two different approaches: the first

considers the work of Réthly [19], the other refers Szeidovitz works with primary sources and estimates of [2], [3] leading to estimate between 6.1 and 6.5 as it is shown in [11], [26]. As to the damage, contemporary sources refer to 91% of damaged buildings in the city of Komárom, in several degrees: 279 completely destroyed, 353 partially collapsed, 213 needed expensive repairs and 219 cheap repairs [14], [15].

Table I

Magnitude (M) estimations of the major seismic events occurred in Hungary [21]

Local	Szombathely	Komárom	Mór	Jászberény	Kecskemét	Eger	Dunaharaszti
Date	456	1763	1811	1868	1911	1925	1956
M	6.6	5.7~6.5	5.4	4.9	5.6	5.3	5.6

3.2. Historical sources and structural damage records

Historical sources exist as official documents [18], depictions (Fig. 4), books [17] and newspaper articles [19]. The *Consilium Locumtenentiale* was ordered to evaluate the damage and quantify the repair costs in the region, resulting in a report entitled *Acta Terrae Motus Anni 1763*, in fascicles A to F (mainly letters). No. 10 of fascicle A focuses on the quantification of costs by city for four different building categories, as shown in Szeidovitz [3]. Religious buildings as churches, parochial houses and chapels compose the first category, castles, palaces and manors the second, public buildings, inns, mills and kilns the third, and taxpayers' houses the fourth. Additionally, Grossinger refers the most damaged buildings as two-story brick public, ecclesiastical or civil houses, rather than simpler and more flexible peasant houses [17].

The sources, regarding [4], lead us into a dichotomy in structural modeling: still existing affected monumental buildings may guarantee a reliable building/damage relation and are relatively well documented, but fall into modeling complexity and lack representativeness. In [27], initial steps were taken to analyze the church of Zsámbék, which has damage descriptions due to the 1763 earthquake. Another path [13] studies simpler and highly representative (in damage numbers) buildings (dwelling houses, mills, kilns, etc.), and low modeling complexity, but generalizes the building/damage relations of perhaps idealized buildings. This paper aims for the second path, although that generalization requires a methodology to generate building archetypes coherent with the historical sources.

4. Archetype generation

The main issue of this paper is how to define building types for DSA. Archetypes are defined as 'structures that fairly represent the range of configurations and properties of the building group of interest' [28]. The interest period is set here for the 18th century or earlier. These buildings were built of earth, adobe, burnt clay or stone masonry, or even wood and the usual seismic resistant structural elements are masonry walls, arches, vaults and wooden frames. Historical buildings can be studied using true-to-form survey, general survey, historical plans, solely on expert opinion or from general

bibliography, for instance [8], [29]. It is from this survey that the qualitative and quantitative analysis and comparison should arise, aiming for the development of a flexible, comprehensive and quantitative approach for generating of structural archetypes for DSA.

4.1. Historical survey of Tata

There is no broad historical building survey of the city of Komárom. Although, Tata holds regional similarities, in terms of architecture and construction techniques, and some of its historical building are surveyed [8] making it a candidate to source the archetypes generation process. From a list of 122 buildings gathered from historical monuments literature [30]-[32] matching the periodization criteria and having available plans [8], [30], 35 were selected (*Table II*). These buildings were organized by function categories and sub-categories (*Fig. 5*), being that the great majority (45%) are dwellings.

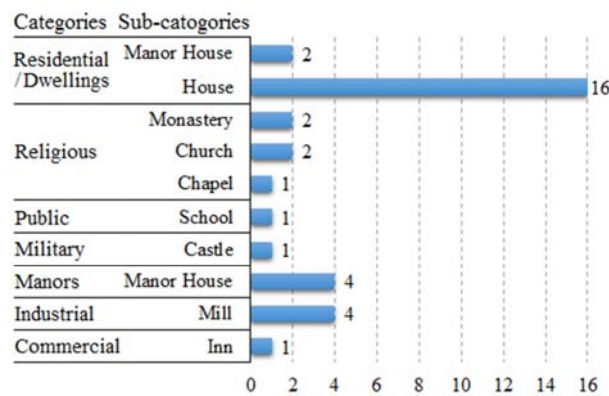


Fig. 5. Categories and sub-categories of the historical survey of Tata [8]

Additionally, their probable location was identified in the first military map (1763-1787, *Fig. 6*) [33], with the help of the survey plans and other city maps. The period of the buildings and intervention descriptions were cross-checked in sources leading to the identification of the buildings in the list and outwit the changes in the street names and urban network [8], [30]. In modern reticular structures, regularities are often associated with typical geometrical parameters as height, span, number of stories, plan area, cross-section dimension, etc. Historical buildings are usually low-rise and contain structural elements of relatively high mass and complexity as self-supporting walls, columns, arches and vaults, i.e. [34], and some difficulties may arise from both the qualitative and quantitative analyses, or by limitations of the surveying method. Therefore, besides the geometrical regularity, historical archetypes require the use of indices similar to those of the real buildings, in order to match their seismic behavior.

Table II

Historical buildings selected from the survey of Tata (T1993) [8] and bibliography: G1959 [30], R1964 [31] and H2006 [32]. The shadowed cells indicate the availability of respective plans

ID	Street name	No.	G1959	R1964	H2006	T1993
1		9	✓	-	-	✓
2	Ady Endre	11	✓	✓	✓	✓
3		22	✓	✓	✓	✓
4		1	✓	✓	✓	-
5	Alkotmány	2	✓	-	✓	✓
6		3	✓	-	✓	✓
7		6	✓	✓	✓	✓
8	Angolkert	-	-	✓	-	✓
9		-	✓	-	-	✓
10	Bajcsy Zsilinszky	24	✓	-	-	✓
11	Bartók Béla	-	✓	-	✓	✓
12		1	-	✓	-	✓
13	Bercsényi	1	✓	✓	✓	✓
14		7	✓	✓	-	✓
15	Fazekas	4	✓	-	-	✓
16		62	✓	✓	✓	✓
17	Fürdő	11	✓	-	✓	✓
18	Hajdú	15	-	-	✓	✓
19		38	✓	-	✓	✓
20	Hősök tér	2	✓	✓	✓	-
21		9/a	✓	✓	✓	✓
22	Kálvária-domb	-	✓	✓	✓	✓
23	Kálvária	4	✓	✓	-	✓
24		-	✓	✓	✓	✓
25	Kossuth tér	6	✓	-	-	✓
26		10	✓	-	-	✓
27		15	✓	-	✓	✓
28	Rákóczi	7	✓	-	-	✓
29		11	✓	-	✓	✓
30	Tanoda tér	5	✓	✓	✓	-
31	Tópart	9	✓	✓	✓	-
32		-	✓	✓	✓	-
33	Váralja	2	-	-	✓	✓
34		3	-	-	✓	✓
35		14	-	-	✓	✓

4.2. Index based archetype definition method

For the quantitative analysis, the use of the in-plan indices from [9], [10] is proposed, together with two new coefficients that should help in the evaluation of the global adequacy of the surveyed buildings for archetype generation. The in-plan directional indices and formulas were applied to guide a simplified pre-analysis guiding intervention priority [10] and then vulnerability analysis of monumental buildings' databases [9], but never for archetype generation. They are based on in-plan areas of the walls, which are seismic resistant in the presence of a horizontal action. This is of particular relevance because they anticipate the seismic strength of the structure, which would be evident in the case of static pushover analysis of the buildings.

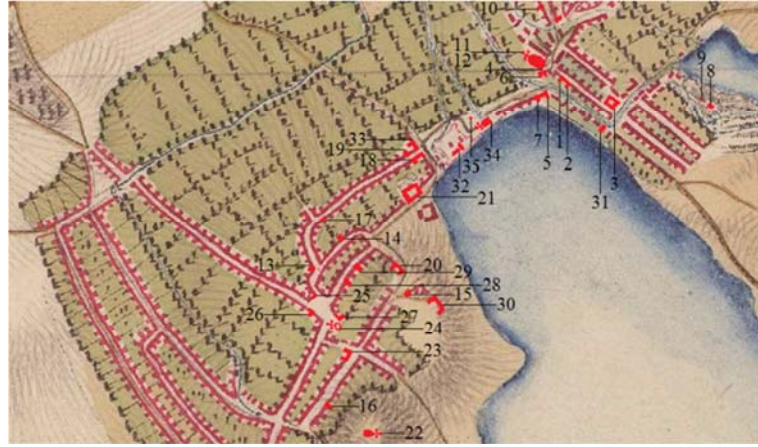


Fig. 6. Location of surveyed buildings in the First Military Map (1763-1787) [33]

The in-plan area ratio (γ_1) is related to the base shear strength and it is the quotient between the in-plane area of the resistant walls ($A_{w,i}$) and the total in-plane area (S). The area-to-weight ratio (γ_2) is given by the horizontal cross-section per unit of weight and it is the quotient between the in-plane area of the resistant walls ($A_{w,i}$) and the quasi-permanent vertical action (G). The base shear ratio (γ_3) provides the safety value with respect to shear and it is the quotient between the seismic action ($F_E = \beta \times G$) and the shear strength of the structure ($V_{Rd,base} = F_{Rd}$), being β the equivalent seismic static coefficient. They are calculated as follows:

$$\gamma_{1,i} = A_{w,i} / S = k_1 \cdot A_{w,i} / A_{w,tot} > 0.10, \quad (1)$$

$$\gamma_{2,i} = A_{w,i} / G = k_2 \cdot A_{w,i} / A_{w,tot} > 1.20 \text{ m}^2 / \text{MN}, \quad (2)$$

$$\gamma_{3,i} = F_{Rd,i} / F_E = k_3 \cdot A_{w,i} / A_{w,tot} > 1.00 \quad (3)$$

with $A_{w,tot} = A_{w,x} + A_{w,y}$, $k_1 = A_{w,tot} / S$, $k_2 = A_{w,tot} / G$ and $k_3 = [\tan \phi + f_{vkl} / (\gamma \times G)] / \beta$. The indices are expected to provide both a pre-evaluation of safety and bounds for archetypes generation.

Furthermore, two more indices are here suggested. While the adequacy ratio (c_1) accounts for how much the target building has been modified, the target to current wall to plan area ratio (c_2) represents the change in material use in the structure of the building. These indices can be calculated using the total wall area (S) and the plan area defined by the outer walls (A_p) for both the target time ($t = t_i$) and the survey, or current time ($t = t_f$), being $\Delta A_p = A_{p,t_f} - A_{p,t_i}$ and $\Delta S = S_{t_f} - S_{t_i}$:

$$c_1 = 1 - \sqrt{\left(\Delta S / S_{t_f}\right)^2 + \left(\Delta A_p / A_{p,t_f}\right)^2}, \quad (4)$$

$$c_2 = \left(S / A_p\right)_{t=t_i} / \left(S / A_p\right)_{t=t_s} - 1. \quad (5)$$

4.3. Illustration of the method

The index framework is applied to the Tata survey, as an example of the process. For this particular case, it is described for the dwelling house with the ID 2 in Ady Endre Street 11, Tata (Fig. 7), in the area of the former city of Tóváros. This building is a paradigmatic example of the application of the methodology because despite its significant modifications over the years, it maintained some of its earlier features, making it possible to identify the baroque walls.

From the L-shaped dwelling in Fig. 7, three intervention periods can be identified, leading to the conclusion that the probable 18th c wall was preserved in the N-W wing of the building. The existence of a division in the characteristically baroque mansard roof and ellipsoidal windows, in this wing (Fig. 7, cut view) also confirms this hypothesis.

Furthermore, the existence of vaulted spaces and a basement suggests that this is probably the oldest part of perhaps a three-cell house. Identified the early building, the table with the input values for the case study is presented.



Fig. 7. Dwelling house of Ady Endre Street 11 [20] and geometric input parameters

Other inputs, material parameters as the density $\gamma=18 \text{ kN/m}^3$, friction angle $\varphi=22^\circ$ cohesion $f_{v,ko}=0.10 \text{ MPa}$ and $\beta=1.00$ are assumed [9], [10]. Additional parameters are also necessary to attain the adequacy ratio. Thus, using the expressions (1)-(5) and the geometrical input parameters in Fig. 7, the in-plan indices ($\gamma_{i,dir}$) may be calculated, as can be seen in Table III.

The quantities as the total weight, $G=2945.75 \text{ kN}$, and the equivalent thickness, $t_{eq}=0.53 \text{ m}$, which was verified to be in between the minimum and maximum thicknesses (t_{min} and t_{max} , Fig. 7). The adequacy ratio was estimated in 14.5% and the wall to plan area ratio shows an increase of 12% in material use in the walls.

Table III

Output parameters and in-plan indices for the Ady Endre 11 dwelling and Archetype A0

ID	Parameters			In-plan area ratio		Area to weight ratio		Base shear ratio	
	k_1	k_2	k_3	$\gamma_{1,x}$	$\gamma_{1,y}$	$\gamma_{2,x}$	$\gamma_{2,y}$	$\gamma_{3,x}$	$\gamma_{3,y}$
2	1.12	14.62	2.51	0.60	0.52	7.81	6.81	1.22	1.07
A0	1.12	21.37	2.19	0.64	0.48	12.23	9.14	2.90	2.17

Despite the identification of the building baroque part, deduced from the survey (Fig. 7, N-W wing), it is not yet an archetype, but the identification of a paradigmatic three cell house (A0, Fig. 8, right) enables its use to judge the previously assumed historical building archetype (section 2, Fig. 2, left), based on [13]. More archetypes are suggested elsewhere [35]. The in-plan ratios were calculated for the archetype (ID A0, Table III) aiming for comparison. An effect that this case is already an archetype results in the adequacy ratio and wall to plan area ratio being $c_1=c_2=0$, respectively. While the indices γ_1 show some similarity, the indices γ_2 and γ_3 , are considerable discrepant, reaching differences of 45% and 63%, respectively. This disparity can be explained by the difference in height (3.80 m and 2.60 m), affecting the self-weight. Thus, regarding the method, the archetype, in its actual state, cannot be considered representative of the presented dwelling, requiring a change in both the height and wall thickness values.

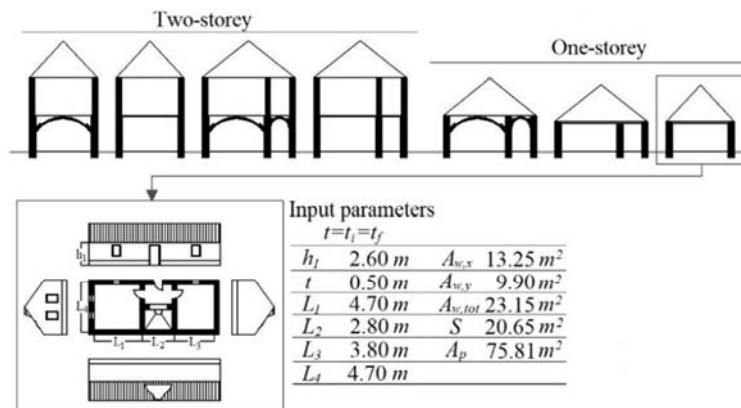


Fig. 8. One and two-storey cuts of building archetypes suggested in [13], and A0 input parameters

5. Conclusion

The present paper established the grounds for the development of an empirical and numerical framework for a method to generate region specific structural archetypes befitting seismic analysis. This approach uses in-plan safety indices that incorporate some of the regularities of the surveyed buildings. Two new indices were introduced in order to frame the adequacy and variation in material use. The generation of structural archetypes for CSM and DSA is an important step for the estimating of the magnitude

of earthquakes using fragility functions and structural damage records. The application of the method to a previously assumed archetype resulted that the archetype mismatched the indexes of the surveyed dwelling, and although the exercise suggests grounds to modify the archetype towards bigger height and wall thickness. A broader composition and completeness of the framework would be required to elaborate broader conclusions.

The Tata historical survey is of considerable importance for it provides a broad empirical source for the generation of archetypes. Although, this study relies on a general historical survey together with historical plans. Therefore, limitations as missing geometry data, non-surveyed parts, and lack of information of the inner core of the structural elements, large variability of the mechanical properties, unknown exact construction sequence and possible joints could be overcome by using a true-to-form survey and by testing the mechanical properties in each surveyed building.

A full analysis of the historical damage records, regarding the magnitude estimation method is not yet done, as well as an estimation of the numbers and types of damaged structures in other cities of the region affected by the 1763 earthquake. Therefore, future developments should provide a full set of archetypes based on the evaluation of the historical damage sources, as well as the results of the DSA of the archetypes.

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