

Electrical cross-talk in rotating ring–disk experiments

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Abstract

The electrical cross-talk between the two working electrodes of generator/collector systems is investigated. Digital simulations are carried out to model simple collection experiments with a rotating ring–disk electrode (RRDE) immersed into a finite resistance solution of a redox couple, where electrical cross-talk may arise due to the shared current routes of the two working electrodes. Based on the analysis of the Kirchhoff (Laplace) matrix of the simulation mesh it is demonstrated that the cross-talk effect is heavily influenced by the selection of the reference point for potential measurements; in practice this is the position of the reference electrode or the tip of the Luggin probe. The devised model is validated by means of a simple and demonstrative experiment.

Keywords: RRDE, ohmic potential drop, digital simulations, Kirchhoff (Laplace) matrix

1. Introduction

In generator/collector (GC) [1] experiments one usually measures stationary detector and collector currents and quantifies the amount of formed products by determining the current ratios. Nowadays, however, transient techniques are also often applied in GC setups like scanning electrochemical microscopy (SECM) [2,3] or the rotating ring–disk electrode (RRDE) [4–7] in order to increase sensitivity or to facilitate the detection of certain products which would otherwise be undetectable by stationary methods. For the same purpose ac-mode

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measurements are sometimes also applied in both configurations [8–13] and yield useful information, for example, on surface-adsorbed intermediates.

GC systems in general provide useful means to detect and quantify the products and side-products of electrode reactions, yet these methods are not without any pitfalls. The aim of this paper is to point out one of these: a certain interference factor, namely the *IR*-drop related electrical cross-talk that can arise between the current-potential characteristics of the working electrodes in practically any four-electrode configurations [14–18]. Cross-talk originates from the shared current routes of the two working electrodes and causes an uncompensated potential shift at one electrode, depending on the current flow of the other one. Cross-talk can, in many cases, lead to serious misinterpretations of the current signals measured in 4-electrode systems. This is especially true if transient perturbations resulting in high currents are applied to either one or both of the working electrodes.

In this paper we propose a digital simulation model of the RRDE system which can account for *IR*-drop related cross-talk and its influence on the results of electrochemical collection experiments. This model can handle any arbitrary potentiostatic (or potentiodynamic) perturbations, and it can also be used to describe four-electrode systems other than the RRDE. After a brief description of the model we present the results of test simulations which are validated by means of a demonstrative experiment. Based on simulation results we also define diagnostic criteria for the detection of electrical cross-talk. Strategies for the elimination of cross-talk and/or the correction of measured data are then suggested.

2. Theory

Several simulation methods were described in the past to study the RRDE system numerically [19–22]. In [22] it was showed that by applying a smooth spatial discretization (a tiling of the space under the RRDE tip into small annulus-shaped cells), and by an accurate numerical solution of the Navier–Stokes equations describing hydrodynamic flow [22,23] it is possible to simulate simple RRDE experiments that very well satisfy some basic theoretical predictions. *I.a.*, it was shown [22] that for a simple collection experiment the simulated limiting currents for the disk closely match the predictions of the Levich equation [24], and there is also a good agreement between simulated and theoretical [25] collection efficiencies.

In the following we show that by solving the equations of Kirchoff's circuit laws over a discrete mesh representing the RRDE system [22] it is possible to carry out simulations that

account for the effects of cross-talk on electrochemical collection experiments. We confine our attention to a system containing two electro-active species (Red and Ox) which, at the working electrodes, can undergo the reaction



We assume that this reaction proceeds reversibly on both the disk and the ring, and thus the concentrations of the Red and Ox species at the vicinities of the working electrodes are always in accordance with the Nernst equation:

$$\frac{c_{\text{Ox near disk or ring}}}{c_{\text{Red near disk or ring}}} = \exp \left[\frac{(\tilde{E}_{\text{disk or ring}} - E^\ominus)F}{RT} \right], \quad (2)$$

where $\tilde{E}_{\text{disk or ring}}$ is a corrected value of the applied potential $E_{\text{disk or ring}}$:

$$\tilde{E}_{\text{disk or ring}} = E_{\text{disk or ring}} - \delta_{IR, \text{disk or ring}}, \quad (3)$$

where $\delta_{IR, \text{disk or ring}}$ denotes an ohmic potential drop, the calculation of which will be described later on. In digital simulations the currents flowing through the working electrodes (I_{disk} and I_{ring}) can be determined knowing the concentration changes in the finite volume simulation cells and the simulation time step t :

$$I_{\text{disk or ring}} = F\Delta t \sum_{\substack{\text{simulation cells} \\ \text{near disk or ring}}} (c_{\text{Ox in cell}}(t) - c_{\text{Ox in cell}}(t - \Delta t))V_{\text{cell}}. \quad (4)$$

As in [22] we apply the method of finite volumes in order to simulate the RRDE system. Both spatial and temporal discretizations are applied, and the algorithm proceeds iteratively. In each time step t the boundary conditions according to equation (2) are realized, which changes the concentrations in the electrode-neighbouring cells of the simulation mesh. The concentration changes are then propagated throughout the entire system as governed by the (discretized) equations of mass transport. (Details about solving the discretized transport equations are given in [19].) The simulation of cross-talk effects is added to this scheme by implementing a downhill simplex root-finding algorithm [26] using which in each simulation step appropriate values of \tilde{E}_{disk} and \tilde{E}_{ring} are determined. These, when used in Equations (2) and (4), give rise to I_{disk} and I_{ring} currents that in turn establish ohmic potential drops ($\delta_{IR, \text{disk}}$ and $\delta_{IR, \text{ring}}$) satisfying Equation (3). Based on I_{disk} and I_{ring} , $\delta_{IR, \text{disk}}$ and $\delta_{IR, \text{ring}}$ are determined by solving Kirchhoff's current laws over the simulation mesh, as it will be shown below.

As a first step, we interpret our simulation mesh as a network of electrical resistors; this concept is illustrated by the graphical abstract of this paper. In case we have a total number of m simulation cells in the mesh, the “equivalent circuit” will contain $n = m + 3$ equipotential nodes due to the three metallic conductors (the disk, the ring and the auxiliary electrode) present in the system. The electric potentials of each node will be ordered in the vector $\boldsymbol{\psi}$; the currents leaving or entering the circuit at each node will be ordered in the vector $\boldsymbol{\iota}$. Since current cannot enter or leave the system, except through the aforementioned electrode metals, $\boldsymbol{\iota}$ will have only three non-zero entries, the sum of which is 0.

There are two types of conductances which can be identified in an equivalent circuit of a simulation mesh. Between each neighbouring cells of the solution, *bulk conductance* values are defined by the κ bulk conductivity of the solution and the geometric parameters of the simulation cells as

$$\sigma = \kappa \frac{A}{d}, \quad (5)$$

where A is the area of the surface between the cells and d the distance of their centre points. We assume that the bulk conductivity κ is constant for the entire system and has no spatial or temporal dependence; i.e., we only consider strongly supported electrolyte solutions.

Aside from bulk conductances there are also *interfacial conductances* present in the equivalent circuit. Although in principle these could be finite (and could even change as the simulation proceeds), here we will assume that their values are infinitely high. This is in agreement with the assumption that all electrode reactions are reversible in the system.

Based on the above considerations, all conductances present in the system are known, and we can construct the $n \times n$ Kirchhoff matrix¹ \mathbf{K} defined as

$$\mathbf{K}_{(j,k)} = \begin{cases} \sigma_{(j,k)} & \text{if } j \neq k \\ -\sum_{j \neq i} \sigma_{(j,i)} & \text{if } j = k. \end{cases} \quad (6)$$

In Equation (6) the term $\sigma_{(j,k)}$ denotes a conductance which directly links nodes j and k of the equivalent circuit. In order to estimate the ohmic drop affecting the two working electrodes, the matrix-vector representation of the equations of Kirchhoff’s current-laws,

$$\mathbf{K}\boldsymbol{\psi} = \boldsymbol{\iota}, \quad (7)$$

¹ In the context of graph theory, the Kirchhoff matrix is often alternatively called the – weighted – Laplace matrix.

has to be solved for ψ . As the inverse of K does not exist [24], we calculate the generalized inverse [27] K^\dagger to obtain the vector of electric potentials as

$$\psi = K^\dagger \iota. \quad (8)$$

Using the K^\dagger matrix it is then possible to obtain the ψ vector in each iteration step from Equation (8). Note that ψ is only determined up to an additive constant, which is due to the fact that K is a positive semi-definite matrix that has exactly one zero eigenvalue with a corresponding element-wise constant eigenvector. Thus the $\delta_{IR,disk}$ and $\delta_{IR,ring}$ terms introduced in Equation (2) are to be defined in the form of a difference:

$$\delta_{IR,disk} = \psi_{disk} - \psi_r, \quad (9.a)$$

$$\delta_{IR,ring} = \psi_{ring} - \psi_r, \quad (9.b)$$

where r ($1 \leq r \leq n^2$) is the index of the equipotential node that we choose as the reference point for voltage measurement. As suggested by Equations (9.a)–(9.b), the position of the reference point (in practice, the location of the tip of the Luggin probe) can have a very deep impact on the current-voltage characteristics of the two working electrodes in RRDE systems.

3. Experimental

In order to demonstrate the effect of IR -drop related cross-talk on the results of simple collection experiments, measurements and simulations were both carried out. A PINE AFE7R8PtPt RRDE was used and measurements were taking place in a cell that contained a solution of $K_3[Fe(CN)_6]$ and $K_4[Fe(CN)_6]$ in equal, $10 \text{ mmol} \cdot \text{dm}^{-3}$ concentrations with $0.5 \text{ mol} \cdot \text{dm}^{-3}$ Na_2SO_4 as a supporting electrolyte. All chemicals were of purissimum grade and purchased from Reanal, Hungary; ultra-pure (Milli-Q) water was used for preparing the solution. In order to assure that the current distribution is as homogeneous as possible, some 10 cm^3 of Hg was placed in the cell, and this “mercury lake” was used as an auxiliary electrode. Saturated calomel electrode (SCE) was used as a reference, and was contacted to the working electrode compartment by the use of a Luggin probe ending in a fine capillary. The Luggin probe itself was filled with the same solution as the working electrode compartment. The entire cell was movable under the RRDE tip, which allowed us to choose different positions of the Luggin probe with respect to the disk and ring. Prior to the measurements, the cell was deaerated using Ar gas.

4. Results and discussion

Simulations were carried out by assuming that Red and Ox are, similarly to the measurement, present in equal ($10 \text{ mmol}\cdot\text{dm}^{-3}$) concentrations. An RRDE geometry identical to that of the PINE AFE7R8PtPt tip (used in the experiments) was considered. The standard potential of the electrode reaction according to Equation (1) was assumed to be $E^\ominus = 0 \text{ V}$ vs. an “ideal” reference electrode.

Figure 1 shows the results of collection experiments and of digital simulation. In both cases cyclic voltammograms (sweep rate: 50 mVs^{-1}) were taken at the disk electrode in a $\pm 325 \text{ mV}$ wide potential window around the open circuit potential value. The ring potential was held at E^\ominus and the ring currents measured simultaneously with the disk voltammograms were plotted vs. E_{disk} . The rotation rate of the RRDE tip was set to 100 min^{-1} .

Simulations and experiments were both carried out by selecting three different reference points for the voltage measurements. In case of the experiments the Luggin probe was set to different positions as shown by the photographs of Figure 1. In the simulations, different values for the r index in Equations (9.a)–(9.b) were chosen so that the situation would mimic the experimental case, and the reference point for voltage measurement would fall directly under the disk (case 1), directly under the ring (case 2) and under the disk but at some greater distance (case 3). Simulations were also carried out in a cross-talk free case 4.

It is apparent in Figure 1 that the position of the Luggin-probe can have a serious effect on the current responses of the two electrodes. If the Luggin probe is set very close to the disk where high currents flow, the recorded ring signal contains a strong distorting component. Less intense cross-talk can be experienced when the Luggin probe is placed close to the ring, while at high distances almost no cross-talk occurs (although the responses of both electrodes are slightly distorted by a “normal IR -drop” [18]). The model presented in Section 2 describes well both the cross-talk and the “normal IR -drop” effects; the results of simulations are in agreement with those of experiment. Based on the results of digital simulations, in what follows we give some rules of thumb that can help experimentalists working with RRDE (or other GC) systems in dealing with the effects of cross-talk:

Diagnostic criteria. A visual comparison of curves recorded with different Luggin probe positions is always advised. Current responses that depend on the position of the Luggin-probe hint to the presence of cross-talk. When using an RRDE it may also be expedient to record curves in the absence of rotation: if the polarization of the disk causes high currents to appear also on a stagnant RRDE ring, this is usually an indication of cross-talk (Figure 2(a)).

Correction of measured curves. Data recorded in the presence of cross-talk may partially be corrected. Consider an experiment (or simulation) that is carried out by placing the Luggin probe close to the ring (case 2 in Figure 1). The measured ring response is in this case almost ideal, while the disk voltammogram is slightly distorted by cross-talk. However, if one determines the pairwise ohmic resistances $R_{\text{disk to ring}}$, $R_{\text{disk to aux}}$ and $R_{\text{ring to aux}}$ (e.g., by means of 2-pole impedance measurements), one can estimate $\delta_{IR, \text{disk}}$ as a function of I_{disk} and I_{ring} (Figure 2(b)) and make corrections to the potential scale of the disk voltammograms. This concept is illustrated by Figure 2(c).

Experimental elimination. Cross-talk (and other IR -drop) effects may be experimentally eliminated by using *two reference electrodes* that target, through two different Luggin probes, the disk and the ring. A suitable bi-potentiostat allowing the connection of two references is needed for this technique. Special care must be taken, however, that hydrodynamic conditions are not disturbed by the probes and no significant screening of the electrodes occur.

5. Conclusion

By solving Kirchhoff's equations over a finite volume simulation mesh of the RRDE system the effect of electrical cross-talk on simple collection experiments was studied. The results of digital simulations were validated by a comparison to measured data. Based on the results of digital simulations, diagnostic criteria as well as correction and elimination strategies were suggested. Similar considerations can also hold for other four-electrode configurations such as SECM (and in some cases also electrochemical STM or conducting-probe AFM).

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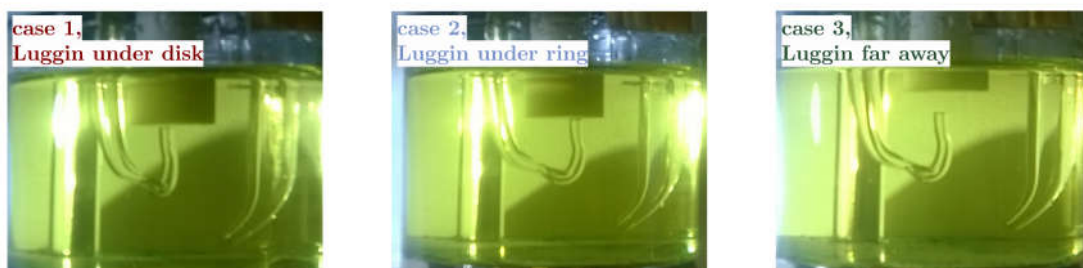
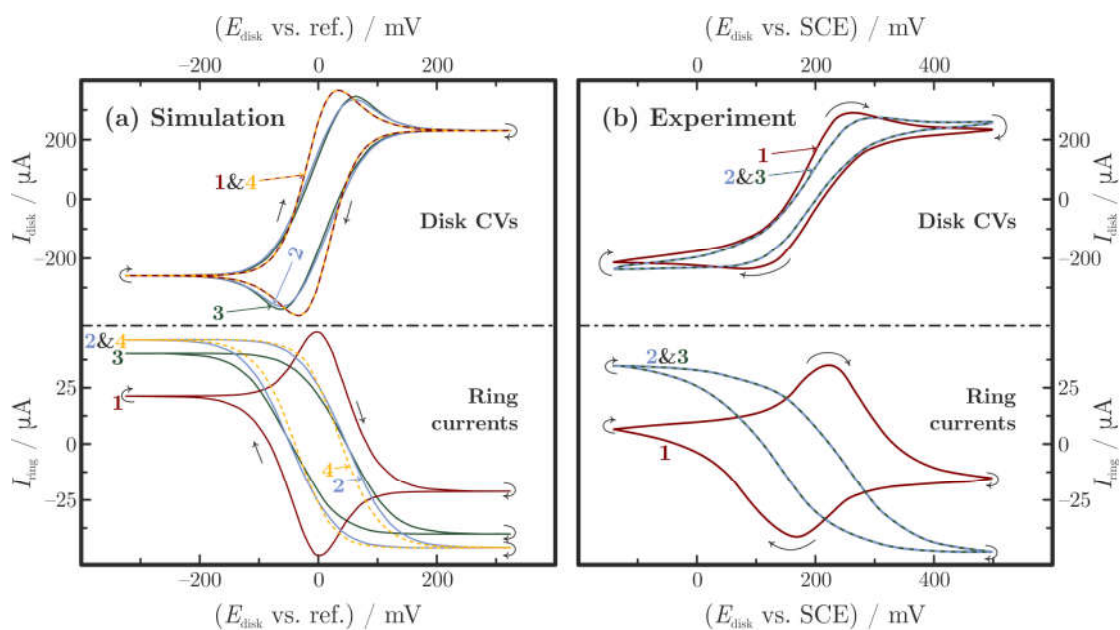


Figure 1. Simulated (a) and measured (b) disk voltammograms and ring currents recorded in parallel with them. The disk is polarized in a ± 325 mV wide potential window around the open circuit potential at a rate of 50 mVs^{-1} . In the meantime the ring is held at E^\ominus . In cases 1, 2 and 3 the Luggin probe takes different positions under the RRDE tip, as illustrated by the photos. In case 4 of the simulation no IR -drop effects were taken into account.

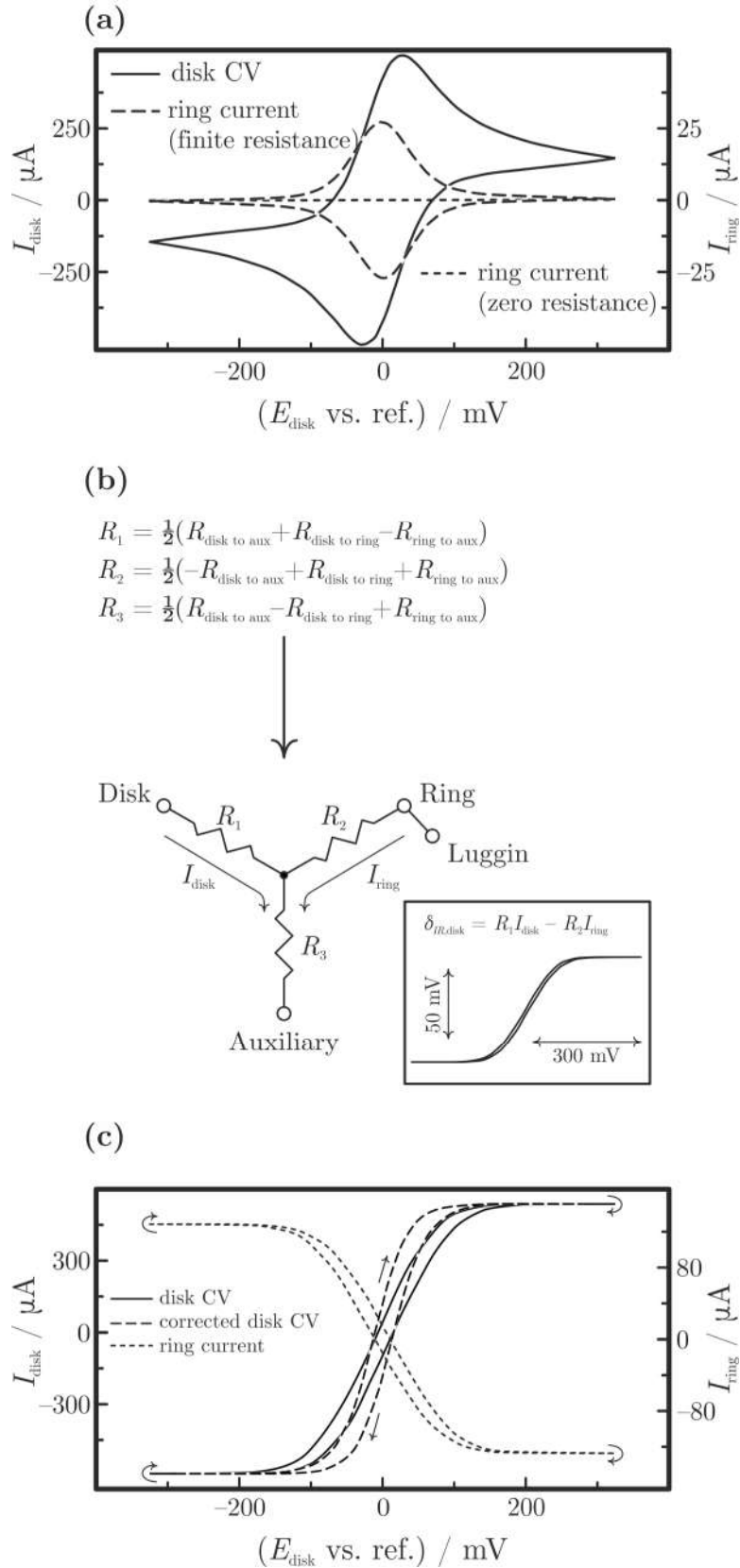


Figure 2. (a) In a cross-talk free case the ring signal on an unrotated RRDE should be practically zero: high currents indicate cross-talk. (b) Simplified equivalent circuit of the RRDE system showing the calculation of $\delta_{IR, \text{disk}}$. (c) By shifting the potential scale of the disk

CVs with $\delta_{IR, disk}$, the disk signal may be corrected for cross-talk effects. Simulation results were obtained at a rotation rate of 500 min^{-1} ; $??\text{mV/s}$ other settings were the same as in case 2 of Figure 1(a).

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